ABSOLUTE MAXIMUM RATINGS

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

ELECTRICAL CHARACTERISTICS

 $(V_+ = 8.2V, V_{\overline{SH}}/SUS = V_{\overline{SH}} = 5.5V$, MINDAC = GND, $T_A = 0^\circ C$ to $+85^\circ C$, unless otherwise noted. Typical values are at $T_A = +25^\circ C$.)

ELECTRICAL CHARACTERISTICS (continued)

(V+ = 8.2V, V_{SH}/SUS = V_{SH} = 5.5V, MINDAC = GND, $T_A = 0^\circ C$ to +85°C, unless otherwise noted. Typical values are at T_A = +25°C.)

ELECTRICAL CHARACTERISTICS (continued)

(V+ = 8.2V, VSH/SUS = VSH = 5.5V, MINDAC = GND, **TA = 0°C to +85°C**, unless otherwise noted. Typical values are at TA = +25°C.)

ELECTRICAL CHARACTERISTICS

 $(V_+ = 8.2V, V_{\overline{\text{SH}}}/\text{SUS} = V_{\overline{\text{SH}}} = 5.5V, \text{ MINDAC} = \text{GND}, \textbf{T_A} = -40^\circ\textbf{C} \textbf{ to } +85^\circ\textbf{C}, \text{ unless otherwise noted.)}$ (Note 6)

Note 1: Corresponds to 512 DPWM cycles or 65536 MODE cycles.

- **Note 2:** When the buck switch is shorted, VCTFB goes high causing V_{CCV} to go below the fault detection threshold.
- **Note 3:** Corresponds to 64 DPWM cycles or 8192 MODE cycles. **Note 4:** The MODE pin thresholds are only valid while the part is
- operating. In shutdown, $V_{REF} = 0$ and the part only differentiates between SMB mode and ADC mode. In shutdown with ADC mode selected, the CRF/SDA and CTL/SCL pins are at high impedance and will not cause extra supply current when their voltages are not at GND or VL.

Note 6: Specifications from -40°C to +85°C are guaranteed by design, not production tested.

Typical Operating Characteristics (continued)

 $(V_{\text{IN}} = 12V, V_{\text{CTL}} = V_{\text{CRF}}, V_{\text{MINDAC}} = 1V, \text{ MODEL} = \text{GND}, \text{ Circuit of Figure 8.}$

*MAX1739/MAX1839***†**

RESIXAM/2571XAM

LAMP-OUT VOLTAGE LIMITING

/VI/IXI/VI

$(V_{IN} = 12V, V_{CTL} = V_{CRF}, V_{MINDAC} = 1V, MODE = GND, Circuit of Figure 8.)$ **VL vs. BATT VOLTAGE VL vs. I_{VL}** 6 5.40 4.6 NORMAL OPERATION MAX1739/1839 toc14 MAX1739/1839 toc14 NORMAL OPERATION 5.35 4.5 5 TIIM SHUTDOWN 5.30 **SHUTDOWN** 4 SHUTDOWN VL (V) 4.4 VL (V) VL (V) 3 5.25 4.3 2 5.20 4.2 5.15 1 4.1 5.10 0.01 4.0 $\boldsymbol{0}$ 0 5 10 15 20 25 0.01 0.1 1 10 100 IVL (mA) V_{BATT} (V)

Typical Operating Characteristics (continued)

MAXIM

8 ___

Pin Description

Detailed Description

The MAX1739/MAX1839 regulate the brightness of a CCFL in three ways:

1) Linearly controlling the lamp current.

2) Digitally pulse-width modulating (or chopping) the lamp current (DPWM).

3) Using both methods simultaneously for widest dimming range.

DPWM is implemented by pulse-width modulating the lamp current at a rate faster than the human eye can

detect. Figure 1 shows the current and voltage waveforms for the three operating modes with the brightness control set to 50% of full scale.

The MAX1739/MAX1839 include a 5.3V linear regulator to power most of the internal circuitry, drivers for the buck and Royer switches, and the synchronizable DPWM oscillator. The MAX1739/MAX1839 are very flexible and include a variety of operating modes, an analog interface, an SMBus interface (MAX1739 only), a shutdown mode, lamp-out detection, and buck-switch short detection.

Figure 1. Brightness Control Methods

Voltage and Current Control Loops

The MAX1739/MAX1839 use two control loops. The current control loop regulates the average lamp current. The voltage control loop limits the maximum average primaryside transformer voltage. The voltage control loop is active during the beginning of DPWM on-cycles and in some fault conditions. Limiting the transformer primary voltage allows for a lower transformer secondary voltage rating that can increase reliability and decrease cost of the transformer. The voltage control loop acts to limit the transformer voltage any time the current control loop attempts to steer the transformer voltage above its limit as set by VCTFB (see *Sense Resistors*).

The voltage control loop uses a transconductance amplifier to create an error current based on the voltage between CTFB and the internal reference level (600mV typ) (Figure 2). The error current is then used to charge and discharge C_{CCV} to create an error voltage VCCV. The current control loop produces a similar signal based on the voltage between CSAV and its internal reference level (see the *Dimming Range* section). This error voltage is called VCCI. The lower of V_{CCV} and V_{CCI} is used with the buck regulator's PWM ramp generator to set the buck regulator's duty cycle.

During DPWM, the two control loops work together to limit the transformer voltage and to allow wide dimming range with good line rejection. During the DPWM offcycle, V_{CCV} is set to 1.2V and CCI is set to high impedance. VCCV is set to 1.2V to create soft-start at the beginning of each DPWM on-cycle in order to avoid overshoot on the transformer primary. V_{CC} is set to high impedance to keep V_{CCI} from changing during the off-cycles. This allows the current control loop to regulate the average lamp current only during DPWM oncycles and not the overall average lamp current.

Upon power-up, V_{CCI} slowly rises, increasing the duty cycle, which provides soft-start. During this time, V_{CCV}, which is the faster control loop, is limited to 150mV above VCCI by the CCV-CLAMP. Once the secondary voltage reaches the strike voltage, the lamp current begins to increase. When the lamp current reaches the regulation point, V_{CCI} reaches steady state. With MIN- $DAC = VL (DPWM disabled)$, the current control loop remains in control and regulates the lamp current.

With MINDAC between REF and GND, DPWM is enabled and the MAX1739/MAX1839 begin pulsing the lamp current. During the on-cycle, V_{CCV} is at 150mV above V_{CCI}. After the on-cycle, V_{CCV} is forced down to 1.2V to provide soft-start at the beginning of the next on-cycle. Also, VCCI retains its value until the beginning of the next on-cycle. When VCCV increases, it causes the buck regulator duty cycle to increase and provides

soft-start. When V_{CCV} crosses over V_{CCI}, the current control loop regains control and regulates the lamp current. VCCV is limited to 150mV above VCCI for the remainder of the on-cycle.

In a lamp-out condition, V_{CCI} increases the primary voltage in an attempt to maintain lamp current regulation. As V_{CCI} rises, V_{CCV} rises with it until the primary voltage reaches its set limit point. At this point, VCCV stops rising and limits the primary voltage by limiting the duty cycle. Because V_{CCV} is limited to 150mV above VCCI, the voltage control loop is quickly able to limit the primary voltage. Without this clamping feature, the transformer voltage would overshoot to dangerous levels because V_{CCV} would take more time to slew down from its supply rail. Once the MAX1739/MAX1839 sense less than 1/6 the full-scale current through the lamp for 2 seconds, it shuts down the Royer oscillator (see *Lamp-Out Detection*).

See the *Sense Resistors* section for information about setting the voltage and current control loop thresholds.

Feed-Forward Control

Both control loops are influenced by the input voltage feed-forward (VBATT) control circuitry of the MAX1739/ MAX1839. Feed-forward control instantly adjusts the buck regulator's duty cycle when it detects a change in input voltage. This provides immunity to changes in input voltage at all brightness levels. This feature makes compensation over wide input ranges easier, makes startup transients less dependent on input voltage, and improves line regulation for short DPWM ontimes.

The MAX1739/MAX1839 feed-forward control is implemented by varying the amplitude of the buck-switch's PWM ramp amplitude. This has the effect of varying the duty cycle as a function of input voltage while maintaining the same VCCI and VCCV. In other words, VBATT feed forward has the effect of not requiring changes in errorsignal voltage (V_{CCI} and V_{CCV}) to respond to changes in VBATT. Since the capacitors only need to change their voltage minimally to respond to changes in VBATT, the controller's response is essentially instantaneous.

Transient Overvoltage Protection from Dropout

The MAX1739/MAX1839 are designed to maintain tight control of the transformer primary under all transient conditions. This includes transients from dropout, where VBATT is so low that the controller loses regulation and reaches maximum duty cycle. Backlight designs will want to choose circuit component values to minimize the transformer turns ratio in order to minimize primary-side currents and I2R losses. To achieve this,

Figure 2. Functional Diagram

allow the circuit to operate in dropout at extremely low battery voltages where the backlight's performance is secondary. All backlight circuit designs can undergo a transient overvoltage condition when the laptop is plugged into the AC adapter and VBATT suddenly increases. The MAX1739/MAX1839 contain a unique clamp circuit on V_{CCI}. Along with the feed-forward circuitry, it ensures that there is not a transient transformer overvoltage when leaving dropout.

The PK_DET_CLAMP circuit limits V_{CCI} to the peaks of the buck-regulator's PWM ramp generator. As the circuit reaches dropout, V_{CCI} approaches the peaks of the PWM ramp generator in order to reach maximum duty cycle. If VBATT decreases further, the control loop loses regulation and V_{CCI} tries to reach its positive supply rail. The clamp circuit on VCCI keeps this from happening, and V_{CCI} rides just above the peaks of the PWM ramp. As VBATT decreases further, the feed-forward PWM ramp generator loses amplitude and the clamp drags V_{CCI} down with it to a voltage below where V_{CCI} would have been if the circuit was not in dropout. When VBATT is suddenly increased out of dropout, VCCI is still low and maintains the drive on the transformer at the old dropout level. The circuit then slowly corrects and increases V_{CCI} to bring the circuit back into regulation.

Buck Regulator

The buck regulator uses the signals from the PWM comparator, the current-limit detection on CS, and DPWM signals to control the high-side MOSFET duty cycle. The regulator uses voltage-mode PWM control and is synchronized to the Royer oscillator. A falling edge on SYNC turns on the high-side MOSFET after a 375ns minimum off-time delay. The PWM comparator or the CS current limit ends the on-cycle.

Interface Selection

Table 1 lists the functionality of SH/SUS, CRF/SDA, and CTL/SCL in each of the three interface modes of the MAX1739/MAX1839. The MAX1739 features both an SMBus digital interface and an analog interface, while the MAX1839 features only the analog interface. Note

that MODE can also synchronize the DPWM frequency (see *Synchronizing the DPWM Frequency*).

Dimming Range

Brightness is controlled by either the analog interface (see *Analog Interface*) or the SMBus interface (see *SMBus Interface*). CCFL brightness is adjusted in three ways:

1) Lamp current control, where the magnitude of the average lamp current is adjusted.

2) DPWM control, where the average lamp current is pulsed to the lamp with a variable duty cycle.

3) A combination of the first two methods.

In each of the three methods, a 5-bit brightness code is generated from the selected interface and is used to set the lamp current and/or DPWM duty cycle.

The 5-bit brightness code defines the lamp current level with ob00000 representing minimum lamp current and ob11111 representing maximum lamp current. The average lamp current is measured across an external sense resistor (see *Sense Resistors*). The voltage on the sense resistor is measured at CSAV. The brightness code adjusts the regulation voltage at CSAV (VCSAV). The minimum average VCSAV is VMINDAC/10, and the maximum average is set by the following formula:

 $VCSAV = VREF \times 31 / 320 + VMINDAC / 320$

which is between 193.75mV and 200mV.

Note that if V_{CSAV} does not exceed 100mV peak (which is about 32mV average) for over 2 seconds, the MAX1739/MAX1839 will assume a lamp-out condition and shut down (see *Lamp-Out Detection*).

The equation relating brightness code to CSAV regulation voltage is:

 $VCSAV = VREF \times n / 320 + VMINDAC \times (32 - n) / 320$

where n is the brightness code.

To always use maximum average lamp current when using DPWM control, set VMINDAC to VREF.

DPWM control works similar to lamp current control in that it also responds to the 5-bit brightness code. A

Table 1. Interface Modes

brightness code of ob00000 corresponds to a 9.375% DPWM duty cycle, and a brightness code of ob11111 corresponds to a 100% DPWM duty cycle. The duty cycle changes by 3.125% per step, except codes ob00000 to ob00011 all produce 9.375% (Figure 3).

To disable DPWM and always use 100% duty cycle, set VMINDAC to VL. Note that with DPWM disabled, the equations above should assume $V_{\text{MINDAC}} = 0$ instead of $V_{\text{MINDAC}} = V_{\text{L}}$. Table 2 lists MINDAC's functionality, and Table 3 shows some typical settings for the brightness adjustment.

In normal operation, VMINDAC is set between 0 and VREF, and the MAX1739/MAX1839 use both lamp current control and DPWM control to vary the lamp brightness (Figure 4). In this mode, lamp current control regulates the average lamp current during a DPWM oncycle and not the overall average lamp current.

Analog Interface and Brightness Code

The MAX1739/MAX1839 analog interface uses an internal ADC with 1-bit hysteresis to generate the brightness code used to dim the lamp (see *Dimming Range*). CTL/SDA is the ADC's input, and CRF/SCL is its reference voltage. The ADC can operate in either positivescale ADC mode or negative-scale ADC mode. In positive-scale ADC mode, the brightness code increas-

Figure 3. DPWM Settings

Table 2. MINDAC Functionality

es from 0 to 31 as V_{CTL} increases from 0 to V_{CRF}. In negative-scale mode, the brightness scale decreases from 31 to 0 as VCTL increases from 0 to VCRF (Figure 5).

The analog interface's internal ADC uses 1-bit hysteresis to keep the lamp from flickering between two codes. VCTL's positive threshold (VCTL(TH)) is the voltage required to transition the brightness code as VCTL increases and can be calculated as follows:

> $VCTL$ (TH) = $(n + 2) / 33 VCF$ (positive-scale ADC mode, MODE = GND) VCL (TH) = (33 - n) / 33 $VCRF$ (negative-scale ADC mode, MODE = REF)

where n is the current selected brightness code. VCTL's negative threshold is the voltage required to transition the brightness code as VCTL decreases and can be calculated as follows:

> $VCL(TH) = n / 33 VCRF$ (positive-scale ADC mode, MODE = GND) VCL (TH) = (31 - n) / 33 $VCRF$ (negative-scale ADC mode, MODE = REF)

Figure 5 shows a graphic representation of the thresholds. CRF/SDA's and CTL/SCL's input voltage range is 2.7V to 5.5V.

Figure 4. Combined Power Level

Table 3. Brightness Adjustment Ranges (for 33:1 Dimming)

Note: The current-level range is solely determined by the MINDAC-to-REF ratio and is externally set.

See *Digital Interface* for instructions on using the SMBus interface.

Synchronizing the DPWM Frequency

MODE has two functions: one is to select the interface mode as described in *Interface Selection*, and the other is to synchronize the DPWM "chopping" frequency to an external signal to prevent unwanted effects in the display screen.

To synchronize the DPWM frequency, connect MODE to VL, REF, or GND through a 10kΩ resistor. Then connect a 500pF capacitor from an AC signal source to MODE as shown in Figure 6. The synchronization range is from 32kHz to 100kHz, which corresponds to a DPWM frequency range of 250Hz to 781Hz (128 MODE pulses per DPWM cycle). High DPWM frequencies limit the dimming range. See *Loop Compensation* for more information concerning high DPWM frequencies.

Royer Oscillator MOSFET Drivers

The MAX1739/MAX1839 directly drive the two external MOSFETs used in the Royer oscillator. This has many advantages over the traditional method that uses bipolar switching and an extra winding on the transformer. Directly driving the MOSFET eliminates the need for an extra winding on the transformer, which reduces cost and minimizes the size of the transformer. Also, driving the switches directly improves commutation efficiency and commutation timing. Using MOSFETs for the switches typically improves overall inverter efficiency due to lower switch drops.

The Royer topology works as a zero voltage crossing (ZVC) detector and switches currents between the two sections of the transformer primary windings. The two windings work alternately, each generating a half wave that is transferred to the secondary to produce the fullwave sinusoidal lamp voltage and current. The MAX1739/MAX1839 detect the zero crossing through the SYNC pin; the threshold is set at 500mV referred to CS and has a typical delay of 50ns. The active switching forces commutation very close to the ZVC point and has better performance than the traditional windingbased ZVC switchover. Commutation can be further

Figure 5. Brightness Code

Figure 6. DPWM Synchronization

optimized using R14 and R15 as shown in Figure 7. The resistor-divider can be used to force commutation as close to the zero-crossing point as possible.

POR and UVLO

The MAX1739/MAX1839 include power-on reset (POR) and undervoltage lockout (UVLO) features. The POR resets all internal registers, such as DAC output, fault conditions, and all SMBus registers. POR occurs when VL is below 1.5V. The SMBus input logic thresholds are designed to meet electrical characteristic limits for VL as low as 3.5V, but the interface will continue to function down to the POR threshold.

The UVLO threshold occurs when VL is below 4.2V (typ) and disables the buck-switch driver.

Low-Power Shutdown

When the MAX1739/MAX1839 are placed in shutdown, all IC functions are turned off except the 5V linear regulator that powers all internal registers and the SMBus interface (MAX1739). The SMBus interface is accessible in shutdown. In shutdown, the linear regulator output voltage drops to about 4.5V and the supply current is 6µA (typ), which is the required power to maintain all internal register states. While in shutdown, lamp-out detection and buck-switch short-circuit detection latches are reset. The device can be placed into shutdown by either writing to the MODE register (MAX1739 SMBus mode only) or with SH/SUS.

Lamp-Out Detection

For safety, during a lamp-out condition, the MAX1739/ MAX1839 limit the maximum average primary-side transformer voltage (see *Sense Resistors*) and shut down the lamp after 2s.

Figure 7. Adjusting the ZVC Detection

The lamp-out detection circuitry monitors VCSAV and shuts down the lamp if V_{CSAV} does not exceed 75mV (typ) within 2 seconds. This circuitry ignores most pulses under 200ns. However, in some cases, a small capacitor is needed at CSAV to prevent noise from tripping the circuitry. This is especially true in noisy environments and in designs with marginal layout.

Ideally, the voltage at CSAV is a half-wave rectified sine wave. In this case, the CSAV lamp-out threshold is as follows:

I MIN = I MAX / 6

where IMIN is the CSAV lamp out threshold, and IMAX is the maximum lamp current (see *Sense Resistors*). *Note:* The formulas assume a worst-case CSAV lamp-out threshold of 100mV and a maximum CSAV average voltage of 200mV.

Use MINDAC or limit the brightness code to prevent setting the lamp current below the CSAV lamp-out threshold.

STATUS1 bit sets when the lamp-out detection circuit shuts down the device.

Buck-Switch Short Fault Detection and Protection

When the buck switch (N1) fails short, there is no voltage limiting on the transformer and the input forces excessive voltage on the transformer secondary. This

*MAX1739/MAX1839***† 8281XAM/0271XAM**

Wide Brightness Range CCFL Backlight Controllers

increases the circuit's demand for current but may not be enough to blow the fuse. With the buck switch shorted, the center tap rises above its regulation point, which causes the CCV amplifier's output (V CCV) to go low. To detect this, the MAX1739/MAX1839 check that V_{CCV} is below 1V at the end of every DPWM period. If this condition persists for over 250ms (or 64 DPWM pulses), the inverter switch commutation is stopped with either DL1 or DL2 on. With the buck switch shorted, this will cause a short circuit with enough current to blow the fuse. If the buck switch is not shorted, then the inverter latches off as in a lamp-out condition.

Both buck-switch short and lamp-out detection will clear the STATUS1 bit in the SMBus interface. STA-TUS1 does not clear immediately but will clear about 2 seconds after the inverter has been forced off (see *Digital Interface*).

Note that once the inverter board fuse has blown, SMBus communications with the part will cease since the MAX1739 will then be without power.

Applications Information

As shown in the standard application circuit (Figure 8), the MAX1739/MAX1839 regulate the current of a 4.5W CCFL. The IC's analog voltage interface sets the lamp brightness with a minimum 20:1 power adjustment range. This circuit operates from a wide supply-voltage range of 7V to 24V. Typical applications include notebook, desktop monitor, and car navigation displays.

CCFL Specifications

To select the correct component values for the MAX1739/MAX1839 circuit, several CCFL parameters (Table 4) and the minimum DC input voltage must be specified.

Royer Oscillator

Components T1, C6, C7, N2A, and N2B form the Royer oscillator. A Royer oscillator is a resonant tank circuit that oscillates at a frequency dependent on C7, the primary magnetizing inductance of T1 (LP), and the impedance seen by the T1 secondary. Figure 8 shows

Figure 8. Standard Application Circuit

a proven application that is useful for a wide range of CCFL tubes and power ranges. Table 5 shows the recommended components for a 4.5W application.

MOSFETs

The MAX1739/MAX1839 require three external switches to operate: N1, N2A, and N2B. N1 is the buck switch; select a logic-level N-channel MOSFET with low R_{DSON} to minimize conduction losses (100m Ω , 30V typ). Also select a comparable-power Schottky diode for D1. N2A/N2B are the Royer oscillator switches that drive the transformer primary; select a dual-logic-level Nchannel MOSFET with low R_{DSON} to minimize conduction losses (100mΩ, 30V typ).

Sense Resistors

R4 and R5 sense the transformer's primary voltage. Figure 9 shows the relationship between the primary and secondary voltage. To set the maximum average secondary transformer voltage, set R5 = 10k Ω , and select R5 according to the following formula:

$$
R4 = R5 \left(\frac{1.5 V_{S(RMS)}}{N} - 1 \right)
$$

where V_S is the maximum RMS secondary transformer voltage (above the strike voltage), and N is the turns ratio of the transformer.

Table 5. Components for the Standard Application Circuit

Table 4. CCFL Specifications

Figure 9. Transformer Primary/Secondary Voltage Relationship Figure 10. Current-Sense Waveforms

The MAX1739/MAX1839 regulate the average current through the CCFL. The current is sensed through the sense resistor (R13) at CSAV. The voltage at CSAV is the half-wave rectified representation of the current through the lamp (Figure 10). The MAX1739/MAX1839 regulate the average voltage at CSAV ($I_{R13, AVG} \times R13$) and are controlled by either the analog interface or the SMBus interface. To set the maximum lamp current, determine R13 as follows:

$R13 = 0.4304 / I_{L, RMS, MAX}$

where I_{L,RMS,MAX} is the maximum RMS lamp current. MINDAC and the wave shape influence the actual maximum RMS lamp current. Use an RMS current meter to make final adjustments to R13.

Loop Compensation

C_{CCI} sets the speed of the current control loop that is used during startup, maintaining lamp current regulation, and during transients caused by changing the lamp current setting. The standard C_{CCI} value is 0.01µF. Larger values limit lamp current overshoot. Smaller values speed up its response to changes in the lamp current setting, but can lead to instability for extremely small values. Very large values of C_{CCI}

increase the delay to strike voltage in DPWM and can cause loss of regulation in the extreme case. Note that very large C_{CCV} can do the same thing.

C6 not only affects loop compensation, but it also affects the waveform shape, overall efficiency, and the maximum necessary secondary transformer voltage. Low values of C6 improve loop stability, especially in systems using a CCFL with a large difference between its restrike voltage and its operating voltage (characteristic of long narrow CCFLs) during DPWM. A low value of C_6 also improves stability when the lamp's operating voltage drops with an increase in lamp current. However, low values of C_6 increase the maximum necessary transformer voltage. C_7 interacts with C_6 and affects the Royer frequency, Royer Q value, and overall efficiency.

C_{CC} sets the speed of the voltage control loop that affects DPWM transients and operation in fault conditions. If DPWM is not used, the voltage control loop should only be active during fault conditions. The standard value of CCCV is 3300pF. Use the smallest value of CCCV necessary to set an acceptable fault transient response and not cause excessive ringing at the beginning of a DPWM pulse. Note that the worst-case fault

transient that C_{CCV} is designed to protect against is open tube at the beginning of DPWM pulses.

Large C_{CCV} values reduce transient overshoots, but can cause loss of regulation at low DPWM duty cycles by increasing the delay to strike voltage. Smaller values of CCCV allow quicker DPWM startups and faster response to fault conditions. Very small values of CCCV make the circuit more susceptible to ringing, and in extreme cases may cause instability. Some ringing is expected between the Royer oscillator and the buck inductor. Some of the ringing can be suppressed by adding a capacitor in parallel with R5. This capacitor should be chosen such that:

 $1 / (2 \times \pi \times R5 \times C) =$ ringing frequency

When using high DPWM frequencies and low DPWM duty cycles, the DPWM on-time is reduced. In some cases, this causes the lamp current transient to exceed the DPWM on-time. In this case, the MAX1739/ MAX1839 lose regulation and the lamp current never reaches the lamp current set point. Supply rejection while operating in this condition is degraded. If the DPWM on-time is short enough, the lamp current does not have enough time to reach the lamp-out threshold and causes a lamp-out detection. To prevent this, decrease the turn-on transient duration (by lowering C_{CCV}), increase the DPWM duty cycle (by limiting the brightness code), or decrease the DPWM frequency (see *Synchronizing the DPWM Frequency*).

DPWM or other "chopping" methods can cause audible noise from some transformers. The transformer should be carefully designed to avoid such behavior.

Dimming Range

The external components required to achieve a dimming range are highly dependent on the CCFL used. The standard application circuit uses a CCFL with stringent requirements. To achieve a 20:1 dimming range, the standard circuit drops slightly more voltage across C6 as it does across the CCFL at the full lamp current setting. This ensures good stability in that circuit with VMINDAC as low as 1V. To further increase the dimming range when using this CCFL, C6 must be increased, which increases the maximum secondary transformer voltage and requires a transformer with a higher voltage rating. Other components (such as the primary transformer inductance and C7) may also need to be adjusted to maintain good waveforms, Royer efficiency, and the desired Royer frequency.

Other Components

The high-side MOSFET driver is powered by the external boosting circuit formed by C5 and D2. Connect BST through a signal-level Schottky diode to VL, and bypass it to LX with a 0.1µF ceramic capacitor. This circuit delivers the necessary power to drive N1 as shown in Figure 8. If a higher gate capacitance MOSFET is used, the size of the bypass capacitor must be increased. The current need at BST is as follows:

$I_{BST} = 1mA d + QT × f$

where d is the buck controller duty cycle (98% max), Q_T is the MOSFET total gate charge, and f is twice the Royer oscillator frequency.

The maximum current through $D2$ (I_D) is:

$$
I_D = I_{\text{BST}} / (1 - d)
$$

D5A and D5B are used to generate the current-sense voltage across R13. The current through these diodes is the lamp current; use a dual-series signal-level diode.

Bypassing and Board Layout

Connect C4 from VL to GND as close as possible with dedicated traces that are not shared with other signal paths. The ground lines should terminate at the GND end of C4: quiet ground, power ground, and lamp current-sense ground. Quiet ground is used for REF, CCV, R5, and MINDAC (if a resistor-divider is used). The power ground goes from the ground of C4 directly to the ground side of C9. Power ground should also supply the return path for D1, N2, and the buck currentsense resistor (from CS to GND, if used). The ground path for R13 should be separate to ensure that it does not corrupt quiet ground and it is not affected by DC drops in the power ground. Refer to the MAX1739 EV kit for an example of good layout.

Digital Interface (MAX1739)

With MODE connected to VL, the CRF/SDA and CTL/SCL pins no longer behave as analog inputs; instead, they function as SMBus-compatible 2-wire digital interfaces. CRF/SDA is the bidirectional data line, and CTL/SCL is the clock line of the 2-wire interfaces corresponding, respectively, to the SMBDATA and SMBCLK lines of the SMBus. The MAX1739 uses the write-byte, read-byte, and receive-byte protocols (Figure 11). The SMBus protocols are documented in System Management Bus Specification v1.08 and are available at www.sbs-forum.org.

The MAX1739 is a slave-only device and responds to the 7-bit address 0b0101101 (i.e., with the RW bit clear indicating a write, this corresponds to 0x5A). The MAX1739 has three functional registers: a 5-bit brightness register (BRIGHT4–BRIGHT0), a 3-bit shutdown mode register (SHMD2–SHMD0), and a 2-bit status register (STATUS1–STATUS0). In addition, the device

Figure 11. SMBus Protocols

has three identification (ID) registers: an 8-bit chip ID register, an 8-bit chip revision register, and an 8-bit manufacturer ID register.

The CRF/SDA and CTL/SCL pins have Schmidt-triggered inputs that can accommodate slow edges; however, the rising and falling edges should still be faster than 1µs and 300ns, respectively.

Communication starts with the master signaling the beginning of a transmission with a START condition, which is a high-to-low transition on CRF/SDA while CTL/SCL is high. When the master has finished communicating with the slave, the master issues a STOP condition (P), which is a low-to-high transition on CRF/SDA while CTL/SCL is high (Figures 10, 11). The bus is then free for another transmission. Figures 12 and 13 show the timing diagram for signals on the 2-wire interface. The address byte, command byte, and data byte are transmitted between the START and STOP conditions. The CRF/SDA state is allowed to change only while CTL/SCL is low, except for the START and STOP conditions. Data is transmitted in 8 bit words and is sampled on the rising edge of CTL/SCL. Nine clock cycles are required to transfer each byte in or out of the MAX1739 since either the master or the slave acknowledges the receipt of the correct byte during the ninth clock. If the MAX1739 receives its correct slave address followed by $R\overline{W} = 0$, it expects to receive 1 or 2 bytes of information (depending on the protocol). If the device detects a start or stop condition prior to clocking in the bytes of data, it considers this an error condition and disregards all of the data. If the transmission is completed correctly, the registers are updated immediately after a STOP (or RESTART) condition. If the MAX1739 receives its correct slave address followed by RW = 1, it expects to clock out the register data selected by the previous command byte.

SMBus Commands

The MAX1739 registers are accessible through several different redundant commands (i.e., the command byte in the read-byte and write-byte protocols), which can

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Figure 12. SMBus Write Timing

Figure 13. SMBus Read Timing

be used to read or write the brightness, SHMD, status, or ID registers.

Table 6 summarizes the command byte's register assignments, as well as each register's power-on state. The MAX1739 also supports the receive-byte protocol for quicker data transfers. This protocol accesses the register configuration pointed to by the last command byte. Immediately after power-up, the data byte returned by the receive-byte protocol is the contents of the brightness register, left justified (i.e., BRIGHT4 will be in the MSB position of the data byte) with the remaining bits containing a 1, STATUS1, and STATUS0.

This gives the same result as using the read-byte protocol with a 0b10XXXXXX (0x80) command. Use caution with shorter protocols in multimaster systems since a second master could overwrite the command byte without informing the first master. During shutdown, the serial interface remains fully functional. The part also supports limited read/write-word protocol. Read-word works similar to read-byte except the second byte returned is 0xFF. Write-word also works similar to writebyte. The second data byte is acknowledged and updated after the first data byte is acknowledged and updated.

Table 6. Commands Description

**The hexadecimal command byte shown is recommended for maximum forward compatibility with future MAXIM products.*

Brightness Register [BRIGHT4–BRIGHT0] (POR = 0b10111)

The 5-bit brightness register corresponds with the 5-bit brightness code used in the dimming control (see *Dimming Range*). BRIGHT4–BRIGHT0 = 0b00000 sets minimum brightness, and BRIGHT4–BRIGHT0 = 0b11111 sets maximum brightness. The SMBus interface does not control whether the device regulates the current by analog dimming, DPWM dimming, or both; this is done by MINDAC (Table 2).

Shutdown-Mode Register [SHMD2–SHMD0] (POR = 0b001)

The 3-bit shutdown-mode register configures the operation of the device when the \overline{SH}/SUS pin is toggled as described in Table 7. The shutdown-mode register can also be used to shut off directly the CCFL, regardless of the SH/SUS state (Table 8).

Status Register [STATUS1–STATUS0] (POR = 0b11)

The status register returns information on fault conditions. If a lamp is not connected to the secondary of the transformer, the MAX1739 will detect that the lamp current has not exceeded the CSAV detection threshold and after 2 seconds will clear the STATUS1 bit (see *Lamp-Out Detection*). The STATUS1 bit is latched; i.e., it will remain 0 even if the lamp-out condition goes away. When $STATUS1 = 0$, the lamp is forced off. $STA-$ TUS0 reports 1 as long as no overcurrent conditions are detected. If an overcurrent condition is detected in any given DPWM period, STATUS0 is cleared for the duration of the following DPWM period. If an overcurrent condition is not detected in any given DPWM period, STATUS0 is set for the duration of the following digital DPWM period. Forcing the CCFL lamp off by entering shutdown, writing to the mode register, or by toggling SH/SUS sets STATUS1.

ID Registers

The ID registers return information on the manufacturer, the chip ID, and the chip revision number. The MAX1739 is the first-generation advanced CCFL controller, and its ChipRev is 0x00. Reading from the MfgID register returns 0x4D, which is the ASCII code for "M" (for Maxim); the ChipID register returns 0x96. Writing to these registers has no effect.

Table 7. SHMD Register Bit Descriptions

Table 8. SH**/SUS and SHMD Register Truth Table**

X = Don't care

Table 9. Status Register Bit Descriptions (Read Only/Writes Have No Effect)

Pin Configurations (continued) **Chip Information**

TRANSISTOR COUNT: 7194

Package Information

QSOP.EPS

P

(The package drawing(s) in this data sheet may not reflect the most current specifications. For the latest package outline information, go to **www.maxim-ic.com/packages**.)

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