

300MHz High-Speed Op Amp

MAX477

ABSOLUTE MAXIMUM RATINGS

Supply Voltage (V _{CC} to V _{EE}).....	12V	CERDIP (derate 8.00mW/°C above +70°C).....	640mW
Differential Input Voltage.....(V _{CC} + 0.3V) to (V _{EE} - 0.3V)		SOT23 (derate 7.1mW/°C above +70°C).....	571mW
Common-Mode Input Voltage.....(V _{CC} + 0.3V) to (V _{EE} - 0.3V)		Operating Temperature Ranges	
Output Short-Circuit Duration to GND.....	Continuous	MAX477E_A.....	-40°C to +85°C
Continuous Power Dissipation (T _A = +70°C)		MAX477EUK.....	-40°C to +85°C
Plastic DIP (derate 9.09mW/°C above +70°C).....	727mW	MAX477MJA.....	-55°C to +125°C
SO (derate 5.88mW/°C above +70°C).....	471mW	Storage Temperature Range.....-65°C to +160°C	
μMAX (derate 4.1mW/°C above +70°C).....	330mW	Lead Temperature (soldering, 10s).....+300°C	

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

DC ELECTRICAL CHARACTERISTICS

(V_{CC} = +5V, V_{EE} = -5V, V_{OUT} = 0, R_L = ∞, T_A = T_{MIN} to T_{MAX}, unless otherwise noted. Typical values are at T_A = +25°C.) (Note 1)

PARAMETER	SYMBOL	CONDITIONS		MIN	TYP	MAX	UNITS
Input Offset Voltage	V _{OS}	MAX477ESA/EPA/EUA/MJA	T _A = +25°C	0.5	2.0	mV	
		MAX477EUK		0.5	2.0		
		MAX477ESA/EPA/EUA/MJA	T _A = T _{MIN} to T _{MAX}		3.0		
		MAX477EUK			5.0		
Input Offset-Voltage Drift	TCV _{OS}			2		μV/°C	
Input Bias Current	I _B	T _A = +25°C		1	3	μA	
		T _A = T _{MIN} to T _{MAX}			5.0		
Input Offset Current	I _{OS}	T _A = +25°C		0.2	1.0	μA	
		T _A = T _{MIN} to T _{MAX}			2.0		
Differential-Mode Input Resistance	R _{IN(DM)}	Either input		1		MΩ	
Common-Mode Input Voltage Range	V _{CM}	T _A = +25°C		±3.0	±3.5	V	
		T _A = T _{MIN} to T _{MAX}		±2.5			
Common-Mode Rejection Ratio	CMRR	T _A = +25°C	V _{CM} = ±3V	70	90	dB	
		T _A = T _{MIN} to T _{MAX}	V _{CM} = ±2.5V	60			
Power-Supply Rejection Ratio	PSRR	V _S = ±4.5V to ±5.5V		70	85	dB	
Open-Loop Voltage Gain	A _{VOL}	V _{OUT} = ±2.0V, V _{CM} = 0V, R _L = 50Ω	MAX477E_A/477MJA	55	65	dB	
			MAX477EUK	50	65		
Output Voltage Swing	V _{OUT}	T _A = +25°C	R _L = ∞	±3.5	±3.9	V	
		T _A = T _{MIN} to T _{MAX}	R _L = 100Ω	±3.0			
			R _L = 50Ω	±2.5			
Minimum Output Current	I _{OUT}	T _A = -40 °C to +85 °C		70	100	mA	
Short-Circuit Output Current	I _{SC}	Short to ground			150	mA	
Open-Loop Output Resistance	R _{OUT}	V _{OUT} = 0, f = DC			0.1	Ω	
Quiescent Supply Current	I _{SY}	T _A = +25°C		8	10	mA	
		MAX477E_-, T _A = T _{MIN} to T _{MAX}			12		
		MAX477MJA, T _A = T _{MIN} to T _{MAX}			14		

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AC ELECTRICAL CHARACTERISTICS

($V_{CC} = +5V$, $V_{EE} = -5V$, $R_L = 100\Omega$, $A_{VCL} = +1$, $T_A = +25^\circ C$, unless otherwise noted.)

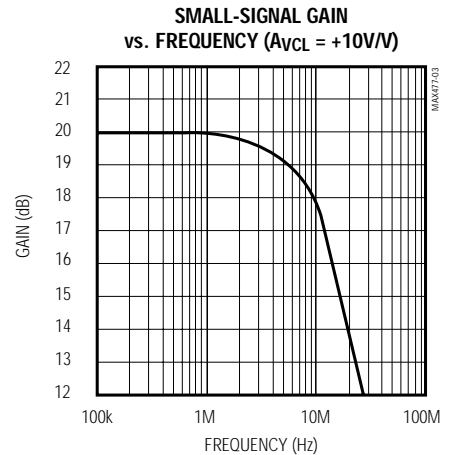
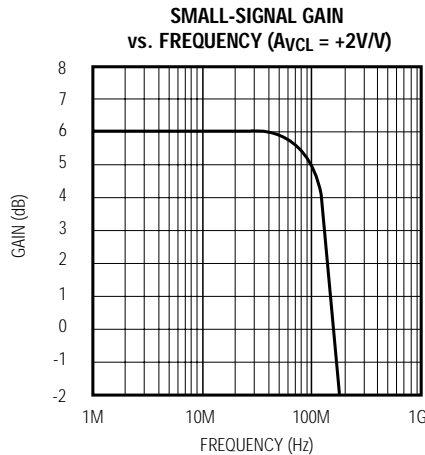
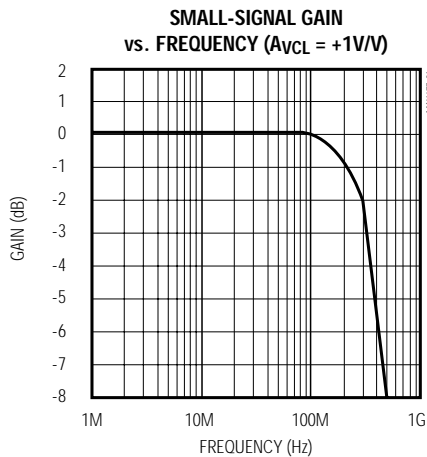
PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS
Small Signal, -3dB Bandwidth	BW-3dB	$V_{OUT} \leq 0.1V_{p-p}$		300		MHz
Small Signal, $\pm 0.1dB$ Gain Flatness	BW0.1dB	$V_{OUT} \leq 0.1V_{p-p}$		130		MHz
Full-Power Bandwidth	FPBW	$V_{OUT} = 2V_{p-p}$		200		MHz
Slew Rate	SR	$V_{OUT} = \pm 2V_{p-p}$		1100		V/ μs
Settling Time	t_s	$V_{OUT} = 2V$ step	to 0.1%	10		ns
			to 0.01%	12		
Rise Time, Fall Time	t_R, t_F	$V_{OUT} = 2V$ step		2		ns
Input Voltage Noise Density	e_n	$f = 10MHz$		5		nV/\sqrt{Hz}
Input Current Noise Density	i_n	$f = 10MHz$, either input		2		pA/\sqrt{Hz}
Differential Gain (Note 2)	DG	$f = 3.58MHz$		0.01		%
Differential Phase (Note 2)	DP	$f = 3.58MHz$		0.01		degrees
Differential-Mode Input Capacitance	$C_{IN(DM)}$	Either input		1		pF
Output Impedance	Z_{OUT}	$f = 10MHz$		2.5		Ω
Total Harmonic Distortion	THD	$f_c = 10MHz$, $V_{OUT} = 2V_{p-p}$		-58		dB
Spurious-Free Dynamic Range	SFDR	$f = 5MHz$, $V_{OUT} = 2V_{p-p}$		-74		dBc
Third-Order Intercept	IP3	$f = 10MHz$, $V_{OUT} = 2V_{p-p}$		36		dBm

Note 1: Specifications for the MAX477EUK (SOT23 package) are 100% tested at $T_A = +25^\circ C$, and guaranteed by design over temperature.

Note 2: Tested with a 3.58MHz video test signal with an amplitude of 40IRE superimposed on a linear ramp (0 to 100IRE). An IRE is a unit of video-signal amplitude developed by the Institute of Radio Engineers. 140IRE = 1V.

Typical Operating Characteristics

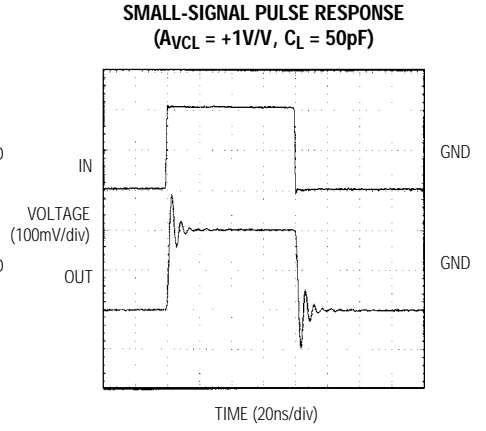
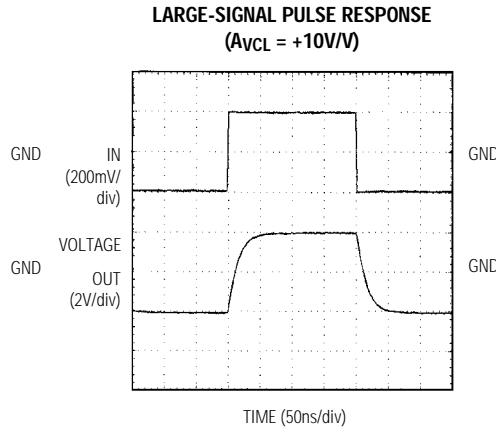
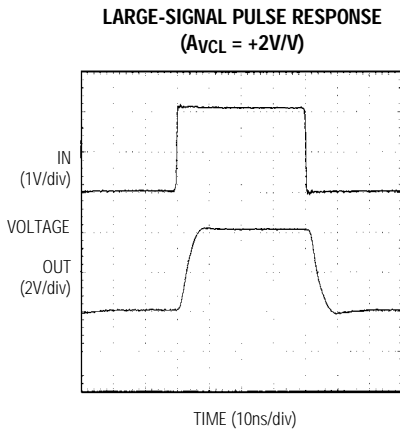
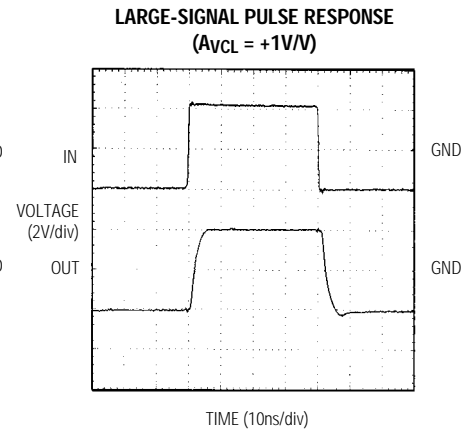
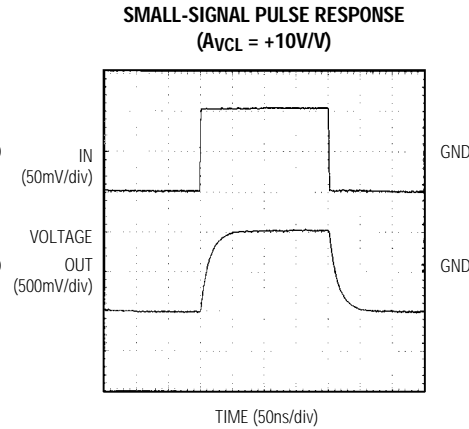
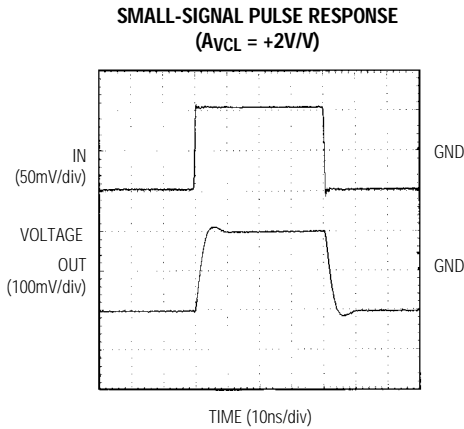
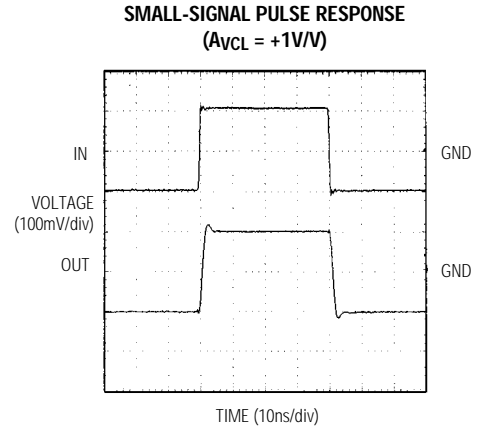
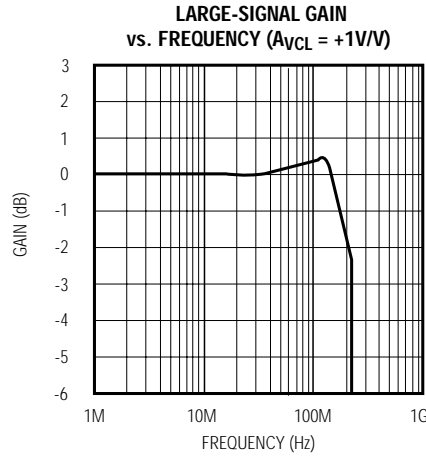
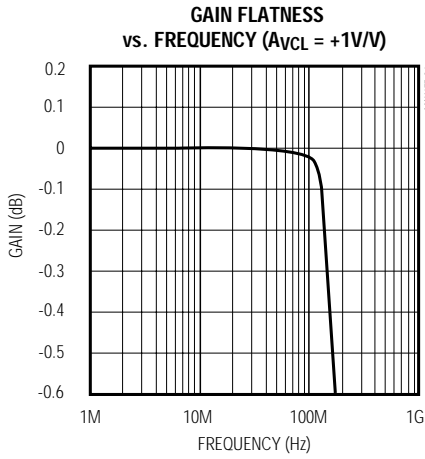
($V_{CC} = +5V$, $V_{EE} = -5V$, $R_L = 100\Omega$, $C_L = 0pF$, $T_A = +25^\circ C$, unless otherwise noted.)



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Typical Operating Characteristics (continued)

($V_{CC} = +5V$, $V_{EE} = -5V$, $R_L = 100\Omega$, $C_L = 0pF$, $T_A = +25^\circ C$, unless otherwise noted.)



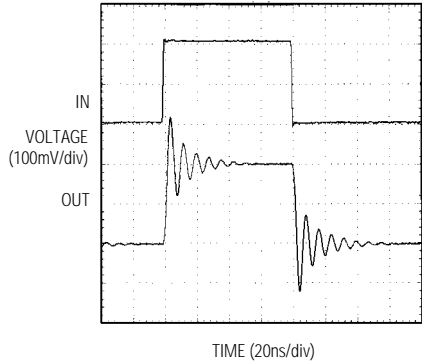
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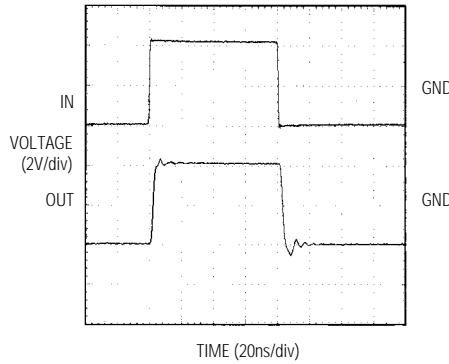
Typical Operating Characteristics (continued)

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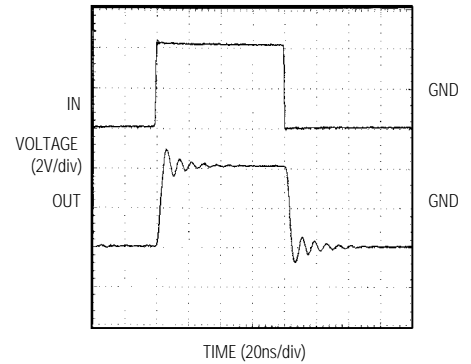
SMALL-SIGNAL PULSE RESPONSE
($A_{vCL} = +1V/V$, $C_L = 100pF$)



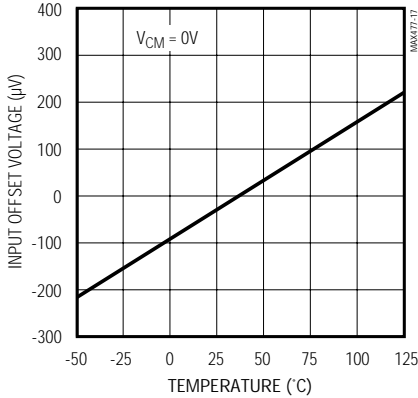
LARGE-SIGNAL PULSE RESPONSE
($A_{vCL} = +1V/V$, $C_L = 50pF$)



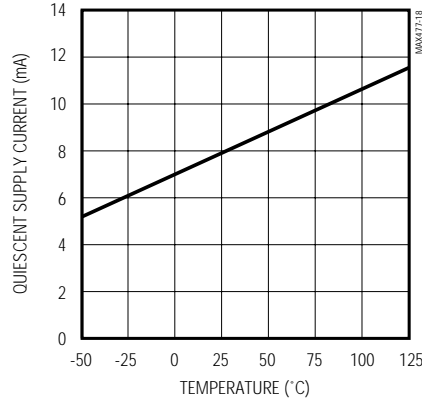
LARGE-SIGNAL PULSE RESPONSE
($A_{vCL} = +1V/V$, $C_L = 100pF$)



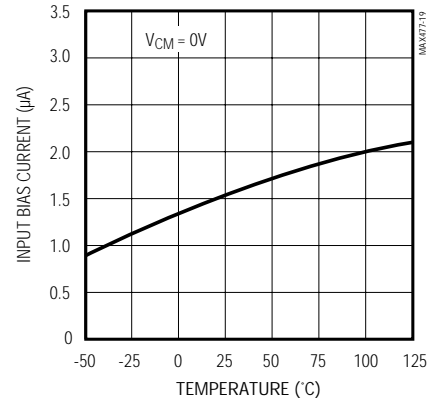
INPUT OFFSET VOLTAGE (V_{OS})
vs. TEMPERATURE



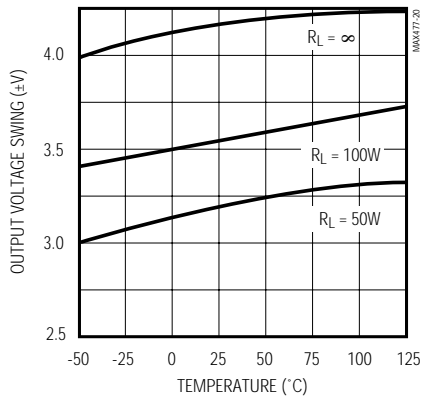
QUIESCENT SUPPLY CURRENT (I_{SY})
vs. TEMPERATURE



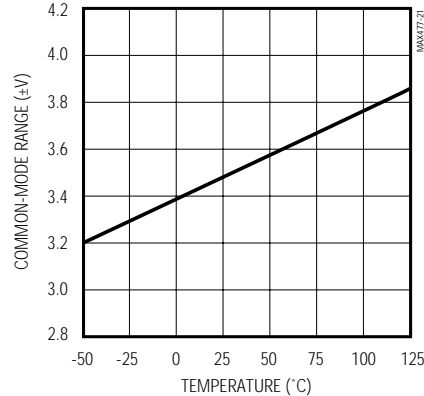
INPUT BIAS CURRENT (I_B)
vs. TEMPERATURE



OUTPUT VOLTAGE SWING
vs. TEMPERATURE



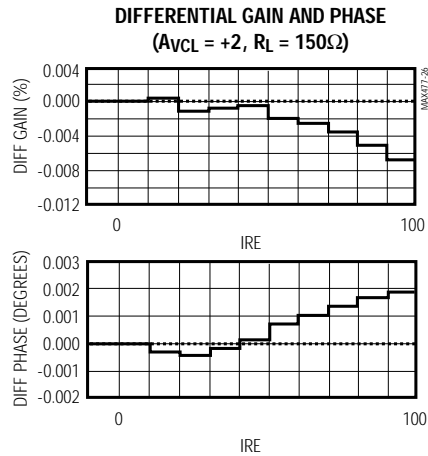
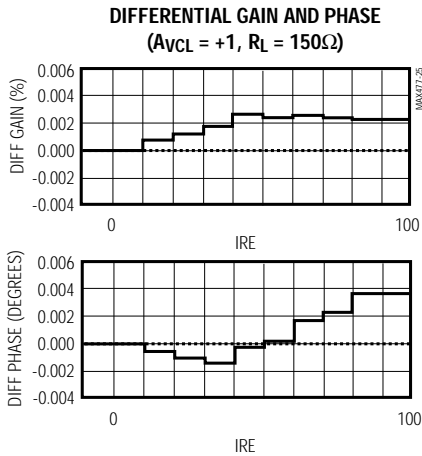
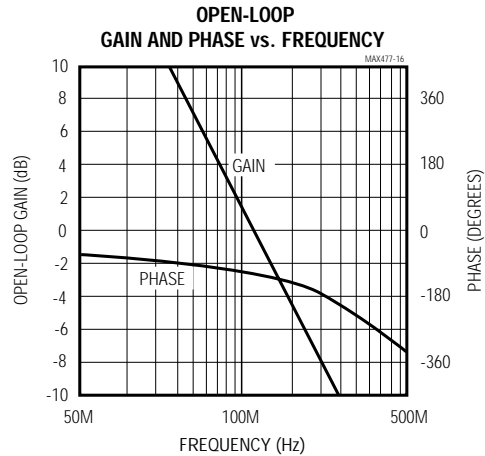
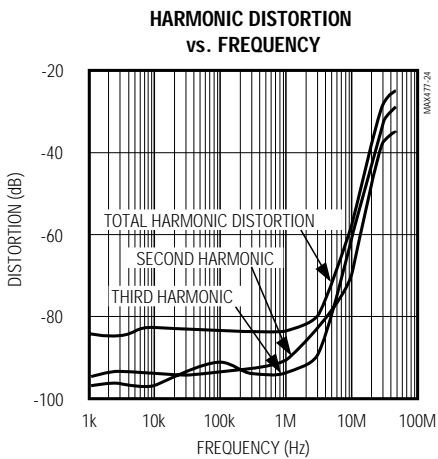
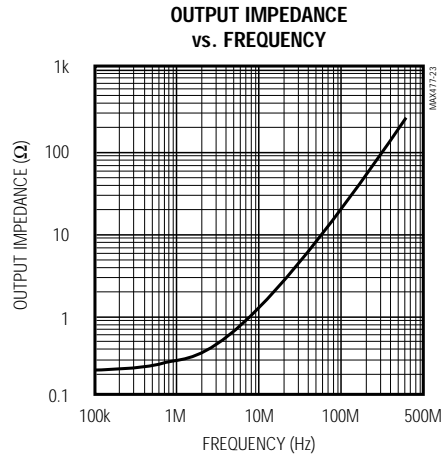
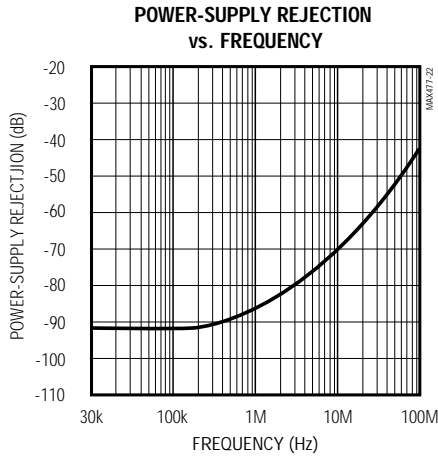
INPUT COMMON-MODE RANGE (V_{CM})
vs. TEMPERATURE



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Typical Operating Characteristics (continued)

($V_{CC} = +5V$, $V_{EE} = -5V$, $R_L = 100\Omega$, $C_L = 0pF$, $T_A = +25^\circ C$, unless otherwise noted.)



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Pin Description

PIN SO/ μ MAX/DIP	SOT23	NAME	FUNCTION
1, 5, 8	—	N.C.	No Connect. Not internally connected.
2	4	IN-	Inverting Input
3	3	IN+	Noninverting Input
4	2	VEE	Negative Power Supply
6	1	OUT	Amplifier Output
7	5	VCC	Positive Power Supply

Detailed Description

The MAX477 allows the flexibility and ease of a classic voltage-feedback architecture while maintaining the high-speed benefits of current-mode feedback (CMF) amplifiers. Although the MAX477 is a voltage-feedback op amp, its internal architecture provides an 1100V/ μ s slew rate and a low 8mA supply current. CMF amplifiers offer high slew rates while maintaining low supply current, but use the feedback and load resistors as part of the amplifier's frequency compensation network. In addition, they have only one input with high impedance.

The MAX477 has speed and power specifications like those of current-feedback amplifiers, but has high input impedance at both input terminals. Like other voltage-feedback op amps, its frequency compensation is independent of the feedback and load resistors, and it exhibits a constant gain-bandwidth product. However, unlike standard voltage-feedback amplifiers, its large-signal slew rate is not limited by an internal current source, so the MAX477 exhibits a very high full-power bandwidth.

Output Short-Circuit Protection

Under short-circuit conditions, the output current is typically limited to 150mA. This is low enough that a short to ground of any duration will not cause permanent damage to the chip. However, a short to either supply will significantly increase the power dissipation and may cause permanent damage. The high output-current capability is an advantage in systems that transmit a signal to several loads. See *High-Performance Video Distribution Amplifier* in the *Applications Information* section.

Applications Information

Grounding, Bypassing, and PC Board Layout

To obtain the MAX477's full 300MHz bandwidth, microstrip and stripline techniques are recommended in most cases. To ensure the PC board does not degrade the amplifier's performance, design the board for a frequency greater than 1GHz. Even with very short traces, use these techniques at critical points, such as inputs and outputs. Whether you use a constant-impedance board or not, observe the following guidelines when designing the board:

- Do not use wire-wrap boards. They are too inductive.
- Do not use IC sockets. They increase parasitic capacitance and inductance.
- In general, surface-mount components have shorter leads and lower parasitic reactance, giving better high-frequency performance than through-hole components.
- The PC board should have at least two layers, with one side a signal layer and the other a ground plane.
- Keep signal lines as short and straight as possible. Do not make 90° turns; round all corners.
- The ground plane should be as free from voids as possible.

Setting Gain

The MAX477 can be configured as an inverting or noninverting gain block in the same manner as any other voltage-feedback op amp. The gain is determined by the ratio of two resistors and does not affect amplifier frequency compensation. This is unlike CMF op amps, which have a limited range of feedback resistors, typically one resistor value for each gain and load setting. This is because the -3dB bandwidth of a CMF op amp is set by the feedback and load resistors. Figure 1a shows the inverting gain configuration and its gain

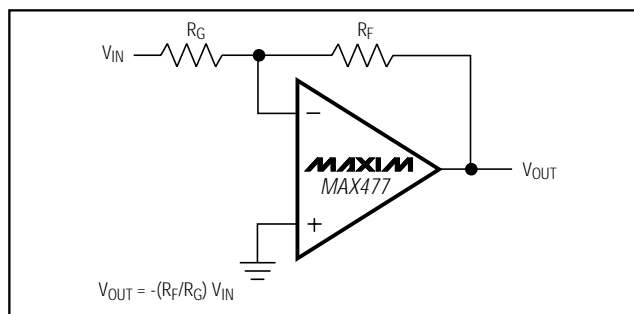


Figure 1a. Inverting Gain Configuration

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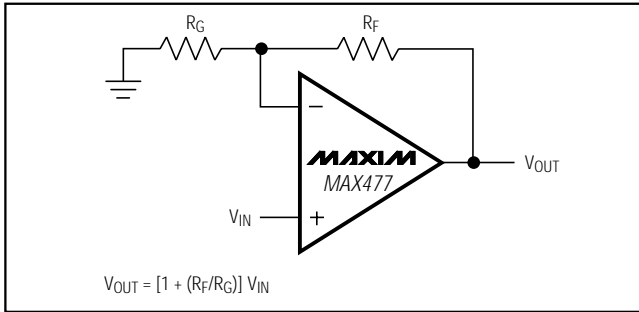


Figure 1b. Noninverting Gain Configuration

equation, while Figure 1b shows the noninverting gain configuration.

Choosing Resistor Values

The feedback and input resistor values are not critical in the inverting or noninverting gain configurations (as with current-feedback amplifiers). However, be sure to select resistors that are small and noninductive.

Surface-mount resistors are best for high-frequency circuits. Their material is similar to that of metal-film resistors, but to minimize inductance, it is deposited in a flat, linear manner using a thick film. Their small size and lack of leads also minimize parasitic inductance and capacitance.

The MAX477's input capacitance is approximately 1pF. In either the inverting or noninverting configuration, excess phase resulting from the pole frequency formed by $R_f \parallel R_g$ and C can degrade amplifier phase margin and cause oscillations (Figure 2). Table 1 shows the recommended resistor combinations and measured bandwidth for several gain values.

DC and Noise Errors

The standard voltage-feedback topology of the MAX477 allows DC error and noise calculations to be done in the usual way. The following analysis shows

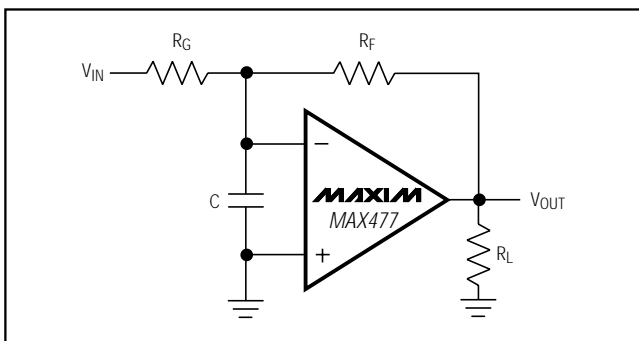


Figure 2. Effect of High-Feedback Resistor Values and Parasitic Capacitance on Bandwidth

Table 1. Resistor and Bandwidth Values for Various Closed-Loop Gain Configurations

GAIN (V/V)	R _g (Ω)	R _f (Ω)	-3dB BANDWIDTH (MHz)
+1	Open	Short	300
+2	500	500	120
+5	125	500	25
+10	50	450	12
-1	300	300	114
-2	150	300	64
-5	100	500	42
-10	50	500	23

that the MAX477's voltage-feedback architecture provides a precision amplifier with significantly lower DC errors and lower noise compared to CMF amplifiers.

1) In Figure 3, total output offset error is given by:

$$V_{OUT} = \left[1 + \frac{R_f}{R_g} \right] \left[V_{OS} + I_B R_S - I_B (R_f \parallel R_g) + I_{OS} (R_S + (R_f \parallel R_g)) \right]$$

For the special case in which R_S is arranged to be equal to $R_f \parallel R_g$, the I_B terms cancel out. Note also, for $I_{OS} (R_S + (R_f \parallel R_g)) \ll V_{OS}$, the I_{OS} term also drops out of the equation for total DC error. In practice, high-speed configurations for the MAX477 necessitate the use of low-value resistors for R_S , R_f , and R_g . In this case, the V_{OS} term is the dominant DC error source.

2) The MAX477's total input-referred noise in a closed-loop feedback configuration can be calculated by:

$$e_T = \sqrt{e_n^2 + e_R^2 + (i_n R_{EQ})^2}$$

where e_n = input-referred noise voltage of the MAX477 (5nV \sqrt{Hz})

i_n = input-referred noise current of the MAX477 (2pA \sqrt{Hz})

R_{EQ} = total equivalent source resistance at the two inputs, i.e., $R_{EQ} = R_S + R_f \parallel R_g$

e_R = resistor noise voltage due to R_{EQ} , i.e.,

$$e_R = \sqrt{4KT R_{EQ}}$$

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As an example, consider $R_S = 75\Omega$, $R_f = R_g = 500\Omega$. Then:

$$R_{EQ} = 75\Omega + (500\Omega \parallel 500\Omega) = 325\Omega$$

$$e_R = \sqrt{4KT} \times 325 = 2.3nV/\sqrt{\text{Hz}} \text{ at } +25^\circ\text{C}$$

$$e_T = \sqrt{(5nV)^2 + (2.3nV)^2 + (2pA \times 325)^2} = 5.5nV\sqrt{\text{Hz}}$$

3) The MAX477's output-referred noise is simply total input-referred noise, e_T , multiplied by the gain factor:

$$e_{OUT} = e_T \left[1 + \frac{R_f}{R_g} \right]$$

In the above example, with $e_T = 5.5nV\sqrt{\text{Hz}}$, and assuming a signal bandwidth of 300MHz (471MHz noise bandwidth), total output noise in this bandwidth is:

$$e_{OUT} = 5.5nV \times \left[1 + \frac{500}{500} \right] \times \sqrt{471\text{MHz}} = 239\mu\text{V}_{\text{RMS}}$$

Note that for both DC and noise calculations, errors are dominated by offset voltage (V_{OS}) and input noise voltage (e_n). For a current-mode feedback amplifier with offset and noise errors significantly higher, the calculations are very different.

Driving Capacitive Loads

The MAX477 provides maximum AC performance with no output load capacitance. This is the case when the MAX477 is driving a correctly terminated transmission line (i.e., a back-terminated 75Ω cable). However, the MAX477 is capable of driving capacitive loads up to 100pF without oscillations, but with reduced AC performance.

Driving large capacitive loads increases the chance of oscillations in most amplifier circuits. This is especially true for circuits with high loop gain, such as voltage followers. The amplifier's output resistance and the load capacitor combine to add a pole and excess phase to the loop response. If the frequency of this pole is low enough and phase margin is degraded sufficiently, oscillations may occur.

A second problem when driving capacitive loads results from the amplifier's output impedance, which looks inductive at high frequency. This inductance forms an L-C resonant circuit with the capacitive load, which causes peaking in the frequency response and degrades the amplifier's gain margin.

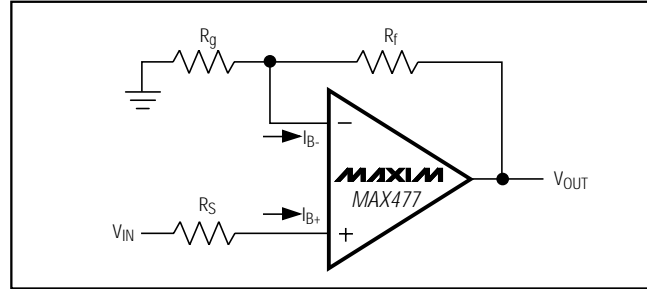


Figure 3. Output Offset Voltage

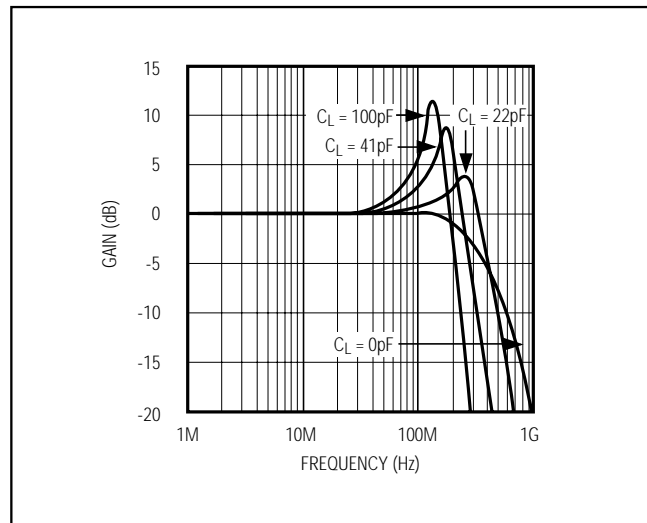


Figure 4. Effect of C_{LOAD} on Frequency Response ($A_{VCL} = +1V/V$)

The MAX477 drives capacitive loads up to 100pF without oscillation. However, some peaking (in the frequency domain) or ringing (in the time domain) may occur. This is shown in Figure 4 and in the Small and Large-Signal Pulse Response graphs in the *Typical Operating Characteristics*.

To drive larger-capacitance loads or to reduce ringing, add an isolation resistor between the amplifier's output and the load, as shown in Figure 5.

The value of R_{ISO} depends on the circuit's gain and the capacitive load. Figure 6 shows the Bode plots that result when a 20Ω isolation resistor is used with a voltage follower driving a range of capacitive loads. At the higher capacitor values, the bandwidth is dominated by the RC network, formed by R_{ISO} and C_L ; the bandwidth of the amplifier itself is much higher. Note that adding an isolation resistor degrades gain accuracy. The load and isolation resistor form a divider that decreases the voltage delivered to the load.

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Flash ADC Preamp

The MAX477's high output-drive capability and ability to drive capacitive loads make it well suited for buffering the low-impedance input of a high-speed flash ADC. With its low output impedance, the MAX477 can drive the inputs of the ADC while maintaining accuracy. Figure 7 shows a preamp for digitizing video, using the 250Msps MAX100 and the 500Msps MAX101 flash ADCs. Both of these ADCs have a 50Ω input resistance and a 1.2GHz input bandwidth.

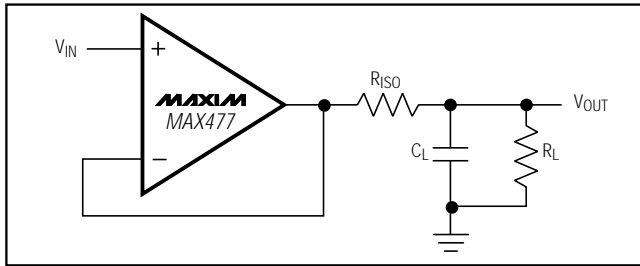


Figure 5. Capacitive-Load Driving Circuit

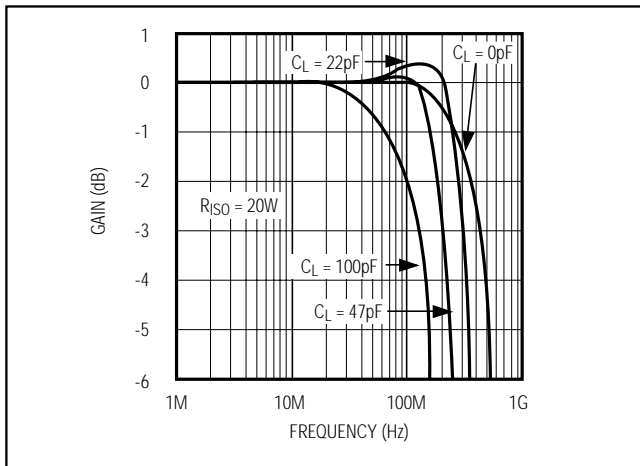


Figure 6. Effect of C_{LOAD} on Frequency Response with Isolation Resistor

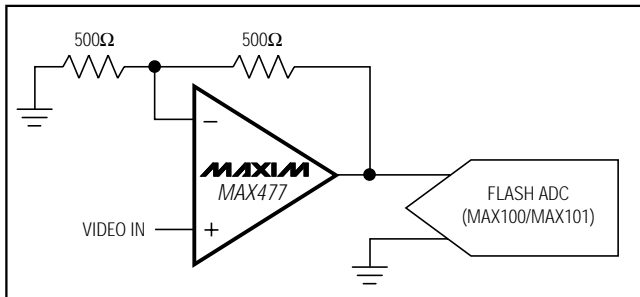


Figure 7. Preamp for Video Digitizer

High-Performance Video Distribution Amplifier

In a gain of +2 configuration, the MAX477 makes an excellent driver for back-terminated 75Ω video coaxial cables (Figure 8). The high output-current drive allows the attachment of up to six $\pm 2V_{p-p}$, 150Ω loads to the MAX477 at $+25^\circ C$. With the output limited to $\pm 1V_{p-p}$, the number of loads may double. The MAX4278 is a similar amplifier configured for a gain of +2 without the need for external gain-setting resistors. For multiple gain-of-2 video line drivers in a single package, refer to the MAX496/MAX497 data sheet.

Wide-Bandwidth Bessel Filter

Two high-impedance inputs allow the MAX477 to be used in all standard active filter topologies. The filter design is straightforward because the component values can be chosen independently of op amp bias. Figure 9 shows a wide-bandwidth, second-order Bessel filter using a multiple feedback topology. The component values are chosen for a gain of +2, a -3dB bandwidth of 10MHz, and a 28ns delay. Figure 10a shows a square-wave pulse response, and Figure 10b shows the filter's frequency response and delay. Notice the flat delay in the passband, which is characteristic of the Bessel filter.

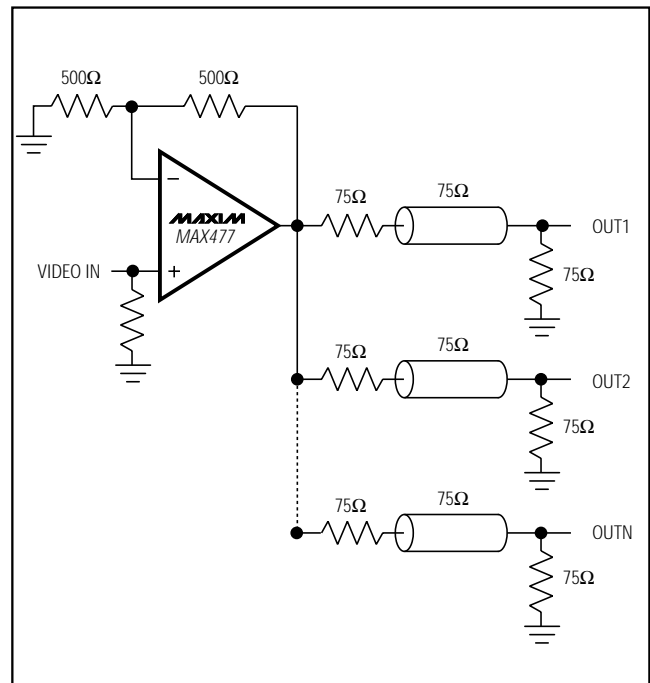


Figure 8. High-Performance Video Distribution Amplifier

300MHz High-Speed Op Amp

Chip Information

MAX477

TRANSISTOR COUNT: 175
SUBSTRATE CONNECTED TO V_{EE}

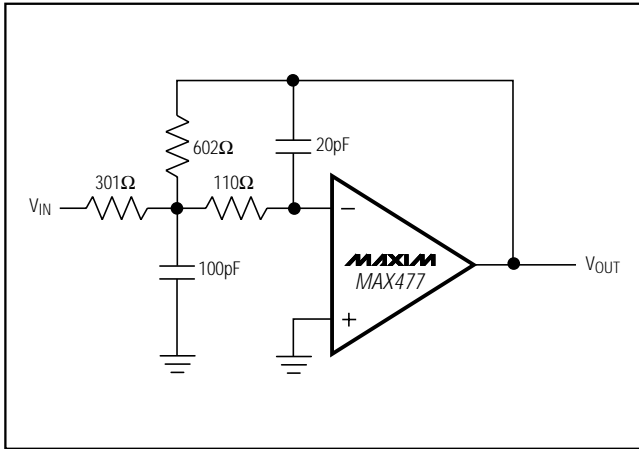


Figure 9. 8MHz Bessel Filter

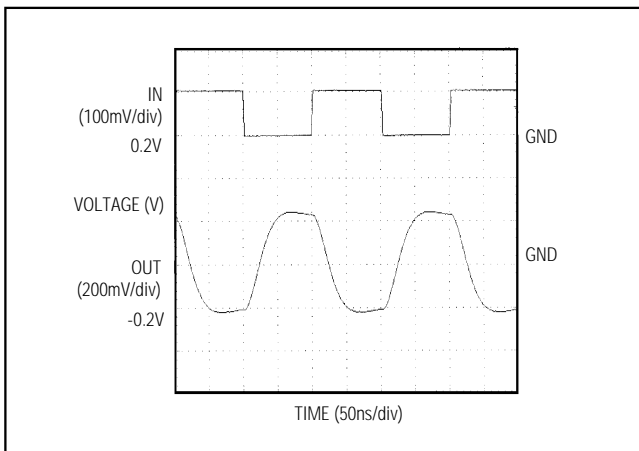


Figure 10a. 5MHz Square Wave Input

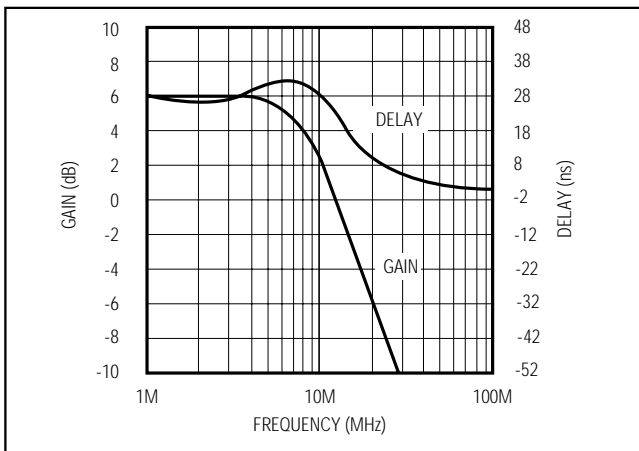
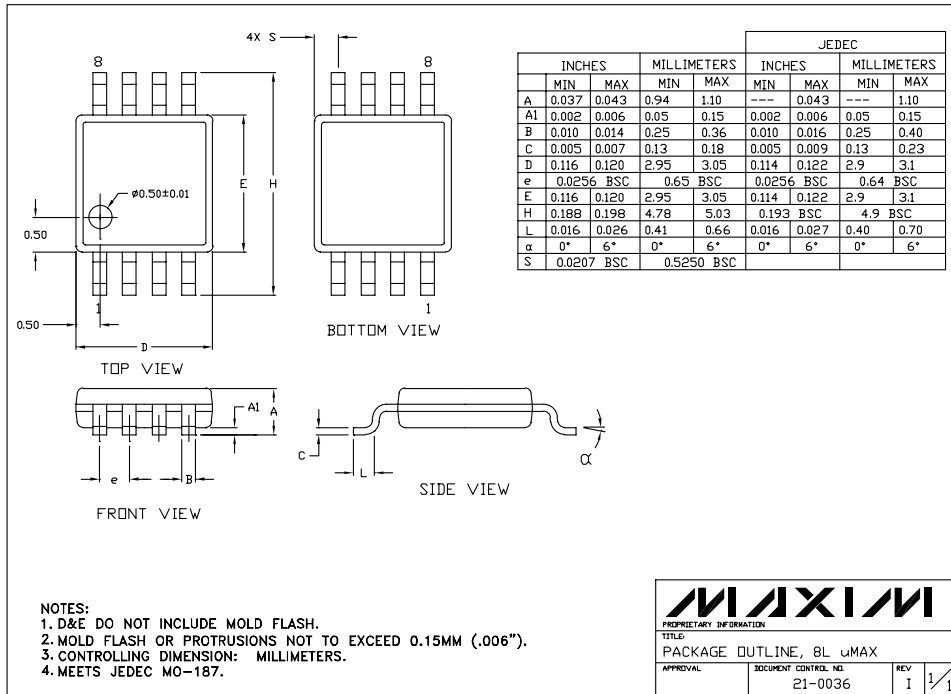


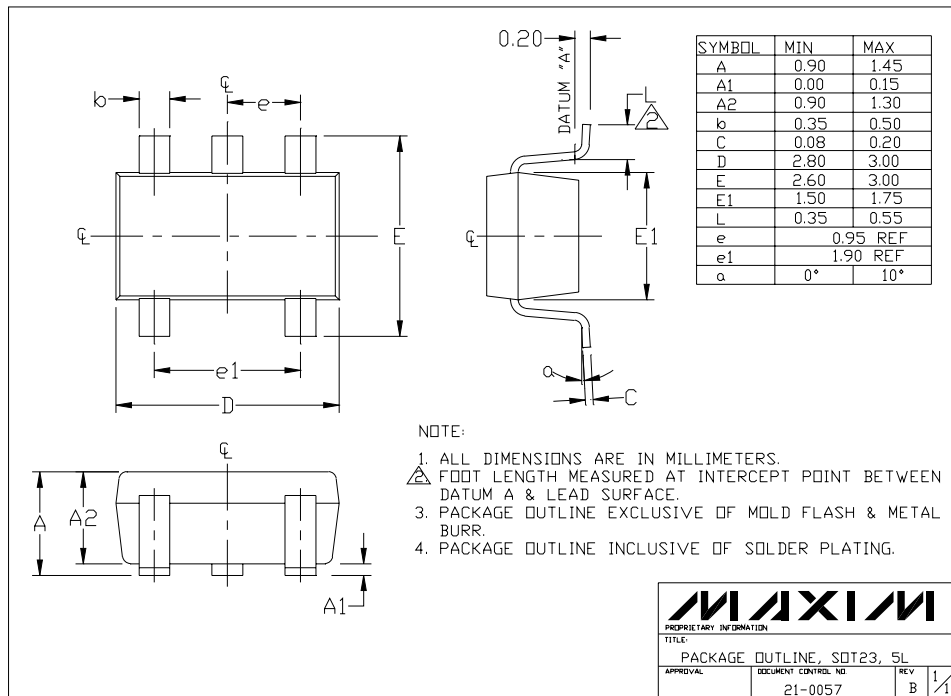
Figure 10b. Gain and Delay vs. Frequency

300MHz High-Speed Op Amp

Package Information



8LUMAXE.PS



SOT23E.PS

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