## **Absolute Maximum Ratings**





*Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these*  or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect<br>device reliability.

### **Electrical Characteristics**





### **Electrical Characteristics (continued)**

(V<sub>CC</sub> = 14V, T<sub>A</sub> = -40°C to +125°C, unless otherwise noted. Typical values are at T<sub>A</sub> = +25°C.) (Note 1)



**Note 1:** 100% production tested at  $T_A$  = +25°C and  $T_A$  = +125°C. Specifications at  $T_A$  = -40°C are guaranteed by design.

## **Typical Operating Characteristics**

( $V_{IN}$  = 14V,  $T_A$  = +25°C, unless otherwise noted.)



### **Typical Operating Characteristics (continued)**

( $V_{IN}$  = 14V,  $T_A$  = +25°C, unless otherwise noted.)



## **Pin Description**





*Figure 1. MAX16010 Monitor Circuit*

### **Detailed Description**

The MAX16010–MAX16014 is a family of ultra-small, low-power, overvoltage-protection circuits for highvoltage, high-transient systems such as those found in automotive, telecom, and industrial applications. These devices operate over a wide 5.5V to 72V supply voltage range, making them also suitable for other applications such as battery stacks, notebook computers, and servers.

The MAX16010 and MAX16011 offer two independent comparators for monitoring both undervoltage and overvoltage conditions. These comparators offer open-drain outputs capable of handling voltages up to 72V. The MAX16010 features complementary enable inputs (EN/ EN), while the MAX16011 features an active-high enable input and a selectable active-high/low OUTB output.

The MAX16012 offers a single comparator and an independent reference output. The reference output can be directly connected to either the inverting or noninverting input to select the comparator output logic.

The MAX16013 and MAX16014 are overvoltageprotection circuits capable of driving two p-channel MOSFETs to prevent reverse-battery and overvoltage conditions. One MOSFET (P1) eliminates the need for external diodes, thus minimizing the input voltage drop. While the second MOSFET (P2) isolates the load or regulates the output voltage during an overvoltage condition. The MAX16014 keeps the MOSFET (P2) latched off until the input power is cycled.

## MAX16010–MAX16014 Ultra-Small, Overvoltage Protection/ Detection Circuits

#### **Voltage Monitoring**

The MAX16010/MAX16011 include undervoltage and overvoltage comparators for window detection (see Figure 1). OUT\_ asserts high when the monitored voltage is within the selected "window." OUTA asserts low when the monitored voltage falls below the lower ( $V_{TRIPLOW}$ ) limit of the window, or OUTB asserts low if the monitored voltage exceeds the upper limit (V<sub>TRIPHIGH</sub>). The application in Figure 1 shows OUT\_ enabling the DC-DC converter when the monitored voltage is in the selected window.

The resistor values (R1–R3) can be calculated as follows:

$$
V_{TRIPLOW} = V_{TH-} \left(\frac{R_{TOTAL}}{R2 + R3}\right)
$$

$$
V_{TRIPHIGH} = V_{TH+} \left(\frac{R_{TOTAL}}{R3}\right)
$$

where  $R_{\text{TOTAL}} = R1 + R2 + R3$ .

Use the following steps to determine the values for R1–R3.

- 1) Choose a value for  $R_{\text{TOTAL}}$ , the sum of R1, R2, and R3. Because the MAX16010/MAX16011 have very high input impedance,  $R_{\text{TOTAL}}$  can be up to 5MΩ.
- 2) Calculate R3 based on  $R_{\text{TOTAL}}$  and the desired upper trip point:

$$
R3 = \frac{V_{TH+} \times R_{TOTAL}}{V_{TRIPHIGH}}
$$

3) Calculate R2 based on  $R_{\text{TOTAL}}$ , R3, and the desired lower trip point:

$$
R3 = \frac{V_{TH+} \times R_{TOTAL}}{V_{TRIPHIGH}}
$$

4) Calculate R1 based on  $R_{\text{TOTAI}}$ , R3, and R2:

$$
R1 = R_{\text{TOTAL}} - R2 - R3
$$

The MAX16012 has both inputs of the comparator available with an integrated 1.30V reference (REF). When the voltage at IN+ is greater than the voltage at IN-, OUT goes high. When the voltage at IN- is greater than the voltage at IN+, OUT goes low. Connect REF to IN+ or IN- to set the reference-voltage value. Use an external resistive divider to set the monitored voltage threshold.



*Figure 2. Typical Operating Circuit for the MAX16012 Figure 3. Overvoltage Limiter Protection*

The MAX16013/MAX16014 can be configured as an overvoltage switch controller to turn on/off a load (see the *Typical Application Circuit*). When the programmed overvoltage threshold is tripped, the internal fast comparator turns off the external p-channel MOSFET (P2), pulling GATE2 to  $V_{CC}$  to disconnect the power source from the load. When the monitored voltage goes below the adjusted overvoltage threshold, the MAX16013 enhances GATE2, reconnecting the load to the power source (toggle ENABLE on the MAX16014 to reconnect the load). The MAX16013 can be configured as an overvoltage-limiter switch by connecting the resistive divider to the load instead of  $V_{CC}$ (Figure 3). See the *Overvoltage Limiter* section.

#### **Supply Voltage**

Connect a 5.5V to 72V supply to  $V_{CC}$  for proper operation. For noisy environments, bypass  $V_{CC}$  to GND with a  $0.1 \mu$ F or greater capacitor. When V<sub>CC</sub> falls below the UVLO voltage, the following states are present (Table 1).



### Table 1. UVLO State (V<sub>CC</sub> < V<sub>UVLO</sub>)



### **Hysteresis**

Hysteresis adds noise immunity to the voltage monitors and prevents oscillation due to repeated triggering when the monitored voltage is near the threshold trip voltage. The hysteresis in a comparator creates two trip points: one for the rising input voltage  $(V_{TH+})$  and one for the falling input voltage ( $V<sub>TH-</sub>$ ). These thresholds are shown in Figure 4.

### **Enable Inputs (EN or EN)**

The MAX16011 offers an active-high enable input (EN), while the MAX16010 offers both an active-high enable input (EN) and an active-low enable input  $(\overline{EN})$ . For the MAX16010, drive EN low or EN high to force the output low. When the device is enabled (EN = high and  $\overline{EN}$  = low) the state of OUTA and OUTB depends on the INA+ and INB- logic states.



*Figure 4. Input and Output Waveforms*



### **Table 2. MAX16011 Output Logic**

For the MAX16011, drive EN low to force OUTA low, OUTB low when LOGIC = low, and OUTB high when LOGIC = high. When the device is enabled  $(EN = high)$ , the state of OUTA and OUTB depends on the INA+, INB-, and LOGIC input (see Table 2).

For the MAX16013/MAX16014, drive EN low to pull GATE2 to  $V_{CC}$ , turning off the p-channel MOSFET (P2). When the device is enabled (EN = high), GATE2 is pulled to the greater of ( $V_{CC}$  - 10V) or GND turning on the external MOSFET (P2).

### **Applications Information**

#### **Input Transients Clamping**

When the external MOSFET is turned off during an overvoltage occurrence, stray inductance in the power path may cause voltage ringing to exceed the MAX16013/ MAX16014 absolute maximum input ( $V_{CC}$ ) supply rating. The following techniques are recommended to reduce the effect of transients:

- Minimize stray inductance in the power path using wide traces, and minimize loop area including the power traces and the return ground path.
- Add a zener diode or transient voltage suppresser (TVS) rated below  $V_{CC}$  absolute maximum rating (Figure 3).

### **Overvoltage Limiter**

When operating in overvoltage-limiter mode, the MAX16013 drives the external p-channel MOSFET (P2), resulting in the external MOSFET operating as a voltage regulator.

During normal operation, GATE2 is pulled to the greater of ( $V_{CC}$  - 10V) or GND. The external MOSFET's drain voltage is monitored through a resistor-divider between the P2 output and SET. When the output voltage rises above the adjusted overvoltage threshold, an internal comparator pulls GATE2 to  $V_{CC}$ . When the monitored

## MAX16010–MAX16014 Ultra-Small, Overvoltage Protection/ Detection Circuits

voltage goes below the overvoltage threshold, the p-channel MOSFET (P2) is turned on again. This process continues to keep the voltage at the output regulated to within approximately a 5% window. The output voltage is regulated during the overvoltage transients and the MOSFET (P2) continues to conduct during the overvoltage event, operating in switched-linear mode.

Caution must be exercised when operating the MAX16013 in voltage-limiting mode for long durations due to the MOSFET's power-dissipation consideration (see the *MOSFET Selection and Operation* section).

#### **MOSFET Selection and Operation (MAX16013 and MAX16014)**

Most battery-powered applications must include reversevoltage protection. Many times this is implemented with a diode in series with the battery. The disadvantage in using a diode is the forward-voltage drop of the diode, which reduces the operating voltage available to downstream circuits ( $V_{\text{LOAD}} = V_{\text{BATTERY}} - V_{\text{DIODE}}$ ). The MAX16013 and MAX16014 include high-voltage GATE1 drive circuitry, allowing users to replace the high-voltage-drop series diode with a low-voltage-drop MOSFET device (as shown in the *Typical Operating Circuit* and Figure 3). The forward-voltage drop is reduced to  $I_{\text{LOAD}}$  x R<sub>DS-ON</sub> of P1. With a suitably chosen MOSFET, the voltage drop can be reduced to millivolts.

In normal operating mode, internal GATE1 output circuitry enhances P1 to a 10V gate-to-source  $(V_{GS})$  for 11V  $V_{\text{CC}}$  < 72V. The constant 10V enhancement ensures P1 operates in a low  $R_{DS-ON}$  mode, but the gate-source junction is not overstressed during high-battery-voltage applications or transients (many MOSFET devices specify a  $\pm 20V$  V<sub>GS</sub> absolute maximum). As V<sub>CC</sub> drops below 10V, GATE1 is limited to GND, reducing P1  $V_{GS}$  to  $V_{CC}$ - GND. In normal operation, the P1 power dissipation is very low:

### $P1 = I_{LOAD}^2 \times R_{DS-ON}$

During reverse-battery applications, GATE1 is limited to GND and the P1 gate-source junction is reverse biased. P1 is turned off and neither the MAX16013/MAX16014 nor the load circuitry is exposed to the reverse-battery voltage. Care should be taken to place P1 (and its internal drain-to-source diode) in the correct orientation for proper reverse-battery operation.

P2 protects the load from input overvoltage conditions. During normal operating modes (the monitored voltage is below the adjusted overvoltage threshold), internal

GATE2 output circuitry enhances P2 to a 10V gate-tosource ( $V$ <sub>GS</sub>) for 11V <  $V_{CC}$  < 72V. The constant 10V enhancement ensures P2 operates in a low  $R_{DS-ON}$ mode, but the gate-to-source junction is not overstressed during high-battery-voltage applications (many pFET devices specify a  $\pm 20V$  V<sub>GS</sub> absolute maximum). As V<sub>CC</sub> drops below 10V, GATE2 is limited to GND, reducing P2 V<sub>GS</sub> to V<sub>CC</sub> - GND. In normal operation, the P2 power dissipation is very low:

#### $P2 = I_{LOAD}2 \times R_{DS-ON}$

During overvoltage conditions, P2 is either turned completely off (overvoltage-switch mode) or cycled off-on-off (voltage-limiter mode). Care should be taken to place P2 (and its internal drain-to-source diode) in the correct orientation for proper overvoltage-protection operation. During voltage-limiter mode, the drain of P2 is limited to the adjusted overvoltage threshold, while the battery  $(V_{CC})$  voltage rises. During prolonged overvoltage events, P2 temperature can increase rapidly due to the high power dissipation. The power dissipated by P2 is:

> $P2 = V_{DS-P2} \times I_{LOAD}$  $=$  (V<sub>CC</sub> - V<sub>OV-ADJUSTED</sub>) x  $I_{\text{LOAD}}$

where  $V_{CC}$  ~  $V_{BATTERY}$  and  $V_{OV-ADJUSTED}$  is the desired load-limit voltage. For prolonged overvoltage events with high P2 power dissipation, proper heatsinking is required.

#### **Adding External Pullup Resistors**

It may be necessary to add an external resistor from  $V_{CC}$ to GATE1 to provide enough additional pullup capability when the GATE1 input goes high. The GATE output can only source up to 1μA current. If the source current is less than 1μA, no external resistor may be necessary. However, to improve the pullup capability of the GATE\_ output when it goes high, connect an external resistor between  $V_{CC}$  and the GATE\_. The application shows a 2MΩ resistor, which is large enough not to impact the sinking capability of the GATE\_ (during normal operation), while providing enough pullup during an overvoltage event. With an 11V (worst case)  $V_{CC}$ -to-gate clamp voltage and a sinking current of 75μA, the smallest resistor should be 11V/75μA, or about 147kΩ. However, since the GATE is typically low most of the time, a higher value should be used to reduce overall power consumption.

**Functional Diagrams**

## MAX16010–MAX16014 Ultra-Small, Overvoltage Protection/ Detection Circuits

## **MAX16010** HYST HYST REGULATOR ENABLE CIRCUITRY 1.23V  $-4V$ INA+ INB-OUTA OUTB GND EN EN  $V_{CC}$

*Figure 5. MAX16010 Functional Diagram*



*Figure 7. MAX16012 Functional Diagram*



*Figure 6. MAX16011 Functional Diagram*



*Figure 8. MAX16013/MAX16014 Functional Diagram*

## **Pin Configurations**



### **Chip Information**

PROCESS: BiCMOS

### **Package Information**

For the latest package outline information and land patterns (footprints), go to **[www.maximintegrated.com/packages](http://www.maximintegrated.com/packages)**. Note that a "+", "#", or "-" in the package code indicates RoHS status only. Package drawings may show a different suffix character, but the drawing pertains to the package regardless of RoHS status.



## **Revision History**



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