

Single/Dual/Quad, 400MHz, Low-Power, Current Feedback Amplifiers

ABSOLUTE MAXIMUM RATINGS

Power-Supply Voltage (V _{CC} to V _{EE}).....	12V	8-Pin μ MAX (derate 4.10mW/°C above +70°C).....	330mW
Input Voltage (IN ₊ , IN ₋).....	(V _{CC} + 0.3V) to (V _{EE} - 0.3V)	14-Pin SO (derate 8.33mW/°C above +70°C).....	667mW
IN ₋ Current (Note 1).....	± 10 mA	16-Pin QSOP (derate 9.52mW/°C above +70°C).....	762mW
Short-Circuit Duration (V _{OUT} to GND)		Operating Temperature Range	
V _{IN} < 1.5V.....	Continuous	MAX41__E__.....	-40°C to +85°C
V _{IN} > 1.5V.....	0sec	Storage Temperature Range.....	-65°C to +160°C
Continuous Power Dissipation (T _A = +70°C)		Lead Temperature (soldering, 10s).....	+300°C
8-Pin SO (derate 5.88mW/°C above +70°C).....	471mW		

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

ELECTRICAL CHARACTERISTICS

(V_{CC} = +5V, V_{EE} = -5V, T_A = T_{MIN} to T_{MAX}, unless otherwise noted. Typical values are at T_A = +25°C.) (Note 1)

PARAMETER	SYMBOL	CONDITIONS		MIN	TYP	MAX	UNITS
DC SPECIFICATIONS (R _L = ∞ , unless otherwise noted)							
Input Offset Voltage	V _{OS}	V _{OUT} = 0V			1	8	mV
Input Offset Voltage Drift	TCV _{OS}	V _{OUT} = 0V			10		μ V/°C
Positive Input Bias Current	I _{B+}	V _{OUT} = 0V, V _{IN} = -V _{OS}			3.5	20	μ A
Negative Input Bias Current	I _{B-}	V _{OUT} = 0V, V _{IN} = -V _{OS}			3.5	20	μ A
Input Resistance		IN+			500		k Ω
		IN-			30		Ω
Input Voltage Noise	e _n	f = 10kHz			2.2		nV/ $\sqrt{\text{Hz}}$
Integrated Voltage Noise	E _{nRMS}	f = 1MHz to 100MHz			27		μ V _{RMS}
Positive Input Current Noise	i _{n+}	f = 10kHz	MAX4112/MAX4117/ MAX4119		13		pA/ $\sqrt{\text{Hz}}$
			MAX4113/MAX4118/ MAX4120		9		
Negative Input Current Noise	i _{n-}	f = 10kHz			14		pA/ $\sqrt{\text{Hz}}$
Common-Mode Input Voltage	V _{CM}			-2.5		2.5	V
Common-Mode Rejection	CMR	V _{CM} = ± 2.5 V		45	50		dB
Power-Supply Rejection	PSR	V _S = ± 4.5 V to ± 5.5 V		60	80		dB
Open-Loop Transimpedance	Z _{OL}	V _{OUT} = ± 2.0 V, V _{CM} = 0V, R _L = 100 Ω		250	500		k Ω
Quiescent Supply Current per Amplifier	I _{SY}	V _{IN} = 0V			5	6.5	mA
Output-Voltage Swing	V _{OUT}	R _L = ∞		± 3.5	± 3.8		V
		R _L = 100 Ω		± 3.1	± 3.5		
Output Current Drive	I _{OUT}	R _L = 30 Ω , T _A = 0°C to +85°C		65	80		mA
AC SPECIFICATIONS (R _L = 100 Ω , unless otherwise noted)							
Small-Signal -3dB Bandwidth	BW _{SS}	V _{OUT} \leq 0.1V _{RMS}	MAX4112/MAX4117		400		MHz
			MAX4113/MAX4119		270		
			MAX4118/MAX4120		300		

Single/Dual/Quad, 400MHz, Low-Power, Current Feedback Amplifiers

ELECTRICAL CHARACTERISTICS (continued)

(V_{CC} = +5V, V_{EE} = -5V, T_A = T_{MIN} to T_{MAX}, unless otherwise noted. Typical values are at T_A = +25°C.) (Note 1)

PARAMETER	SYMBOL	CONDITIONS	MIN	TYP	MAX	UNITS
AC SPECIFICATIONS (R _L = 100Ω, unless otherwise noted) (continued)						
0.1dB Gain Flatness	BW _{0.1dB}	MAX4112/MAX4117/MAX4119, Av _{CL} = +2		100		MHz
		MAX4113/MAX4118/MAX4120, Av _{CL} = +8		115		
Large-Signal -3dB Bandwidth	BW _{LS}	V _{OUT} = 2V _{P-P}	MAX4112/MAX4117	280		MHz
			MAX4119	145		
			MAX4113/MAX4118/ MAX4120	240		
Slew Rate	SR	-2V ≤ V _{OUT} ≤ 2V	MAX4112/MAX4117/ MAX4119	1200		V/μs
			MAX4113/MAX4118/ MAX4120	1800		
Settling Time	t _s	to 0.1%, -1V ≤ V _{OUT} ≤ 1V	MAX4112/MAX4117/ MAX4119	15		ns
			MAX4113/MAX4118/ MAX4120	10		
		to 0.01%, -1V ≤ V _{OUT} ≤ 1V	MAX4112/MAX4117/ MAX4119	35		
			MAX4113/MAX4118/ MAX4120	25		
Rise/Fall Times	t _R , t _F	10% to 90%, -2V ≤ V _{OUT} ≤ 2V		3		ns
		10% to 90%, -50mV ≤ V _{OUT} ≤ 50mV		0.8		
Differential Gain	DG	f = 3.58MHz, R _L = 150Ω	MAX4112/MAX4117/ MAX4119, Av _{CL} = +2	0.02		%
			MAX4113/MAX4118/ MAX4120, Av _{CL} = +8	0.02		
Differential Phase	DP	f = 3.58MHz, R _L = 150Ω	MAX4112/MAX4117/ MAX4119, Av _{CL} = +2	0.03		degrees
			MAX4113/MAX4118/ MAX4120, Av _{CL} = +8	0.04		
Input Capacitance	C _{IN}			2		pF
Output Impedance	Z _{OUT}	f = 10MHz, Av _{CL} = +2		0.9		Ω
Spurious-Free Dynamic Range	SFDR	f _C = 5MHz, V _{OUT} = 2V _{P-P}	MAX4112/MAX4117/ MAX4119, Av _{CL} = +2	-68		dBc
			MAX4113/MAX4118/ MAX4120, Av _{CL} = +8	-62		
Two-Tone Third-Order Intercept	IP ₃	MAX4112/MAX4117/MAX4119, f _C = 10MHz, f _{C1} = 10.1MHz, Av _{CL} = +2		36		dB
Crosstalk		All hostile, V _{IN} = 1V _{P-P} , f = 10MHz		-75		dB

Note 1: The MAX4112/MAX4113/MAX4117-MAX4120 are designed to operate in a closed-loop configuration in which the IN- pin is driven by the OUT pin through an external feedback network. If an external voltage source is connected to IN-, current into or out of IN- must be limited to ±10mA, to prevent damage to the part.

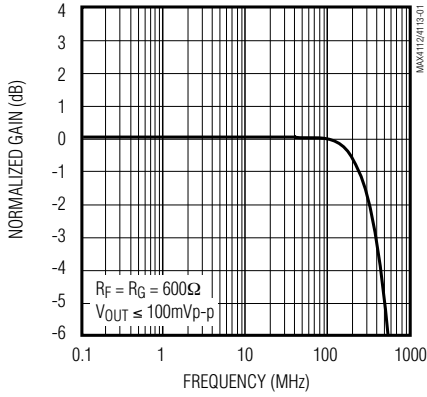
MAX4112/MAX4113/MAX4117-MAX4120

Single/Dual/Quad, 400MHz, Low-Power, Current Feedback Amplifiers

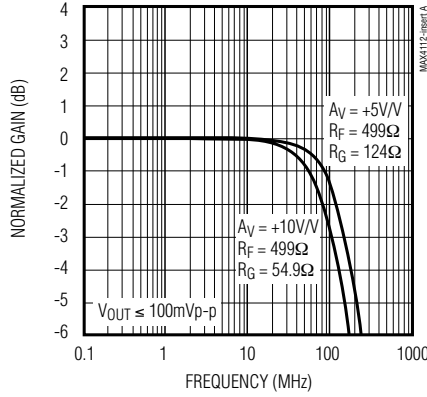
Typical Operating Characteristics

($V_{CC} = +5V$, $V_{EE} = -5V$, $R_F = 499\Omega$, $R_L = 100\Omega$, $T_A = +25^\circ C$, unless otherwise noted.)

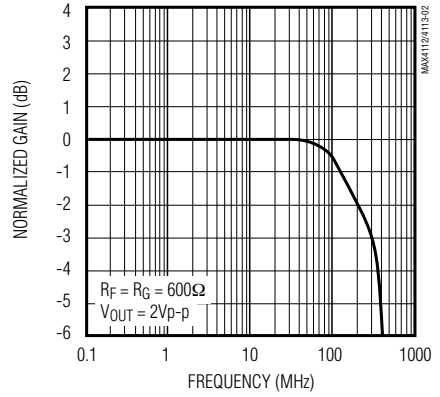
**MAX4112/MAX4117/MAX4119
SMALL-SIGNAL GAIN vs. FREQUENCY
($A_{VCL} = +2$)**



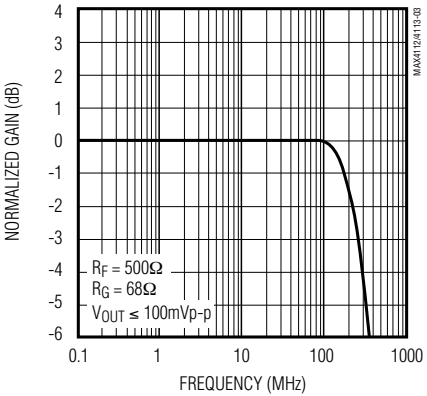
**MAX4112/MAX4117/MAX4119
SMALL-SIGNAL GAIN vs. FREQUENCY
($A_{VCL} = +5, +10$)**



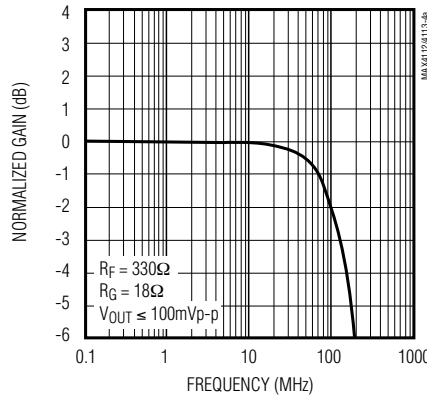
**MAX4112/MAX4117/MAX4119
LARGE-SIGNAL GAIN vs. FREQUENCY
($A_{VCL} = +2$)**



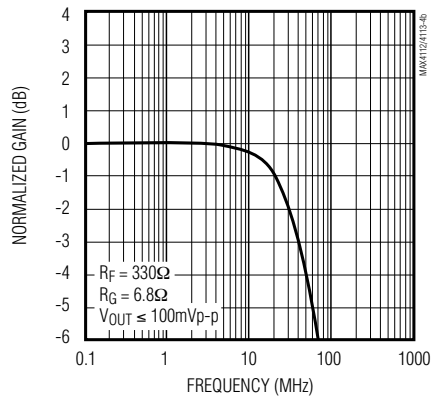
**MAX4113/MAX4118/MAX4120
SMALL-SIGNAL GAIN vs. FREQUENCY
($A_{VCL} = +8$)**



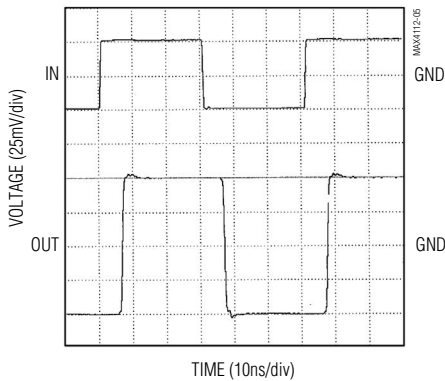
**MAX4113/MAX4118/MAX4120
SMALL-SIGNAL GAIN vs. FREQUENCY
($A_{VCL} = +20$)**



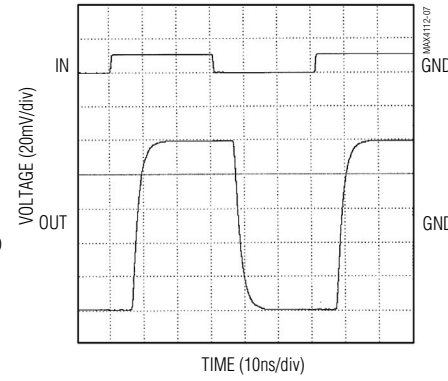
**MAX4113/MAX4118/MAX4120
SMALL-SIGNAL GAIN vs. FREQUENCY
($A_{VCL} = +50$)**



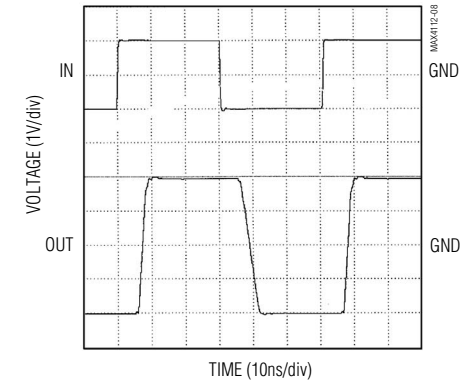
**MAX4112/MAX4117/MAX4119
SMALL-SIGNAL PULSE RESPONSE
($A_{VCL} = +2$)**



**MAX4112/MAX4117/MAX4119
SMALL-SIGNAL PULSE RESPONSE
($A_{VCL} = +10$)**



**MAX4112/MAX4117/MAX4119
LARGE-SIGNAL PULSE RESPONSE
($A_{VCL} = +2$)**

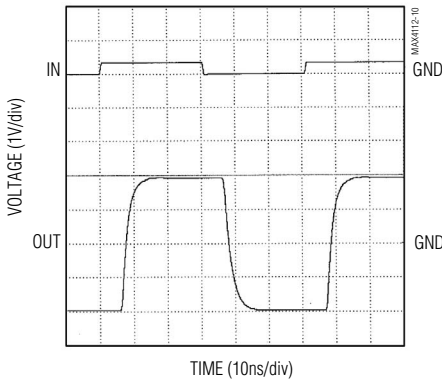


Single/Dual/Quad, 400MHz, Low-Power, Current Feedback Amplifiers

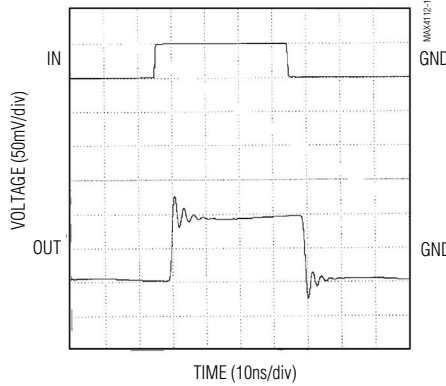
Typical Operating Characteristics (continued)

($V_{CC} = +5V$, $V_{EE} = -5V$, $R_F = 499\Omega$, $R_L = 100\Omega$, $T_A = +25^\circ C$, unless otherwise noted.)

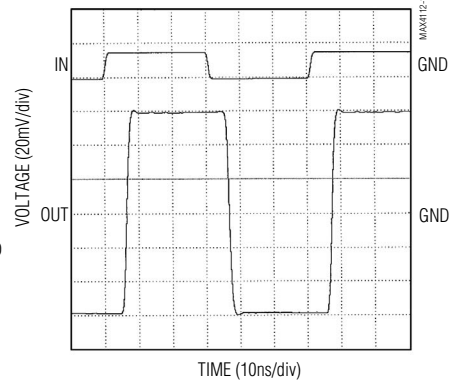
**MAX4112/MAX4117/MAX4119
LARGE-SIGNAL PULSE RESPONSE
($A_{vCL} = +10$)**



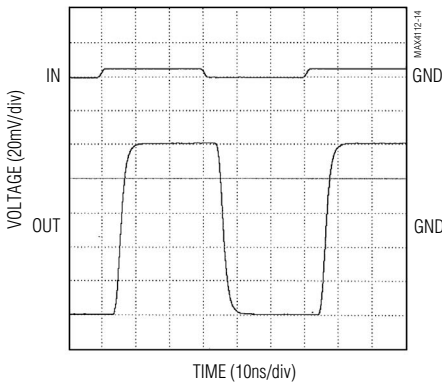
**MAX4112/MAX4117/MAX4119
SMALL-SIGNAL PULSE RESPONSE
($A_{vCL} = +2$, $C_L = 10pF$)**



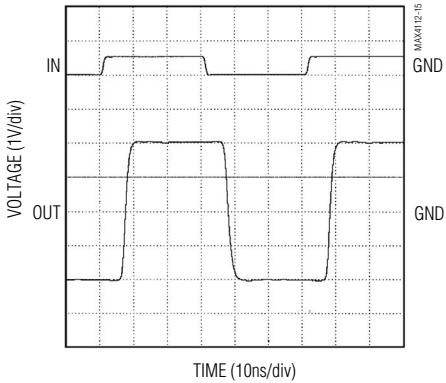
**MAX4113/MAX4118/MAX4120
SMALL-SIGNAL PULSE RESPONSE
($A_{vCL} = +8$)**



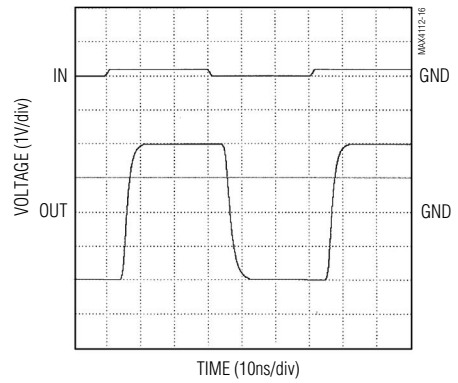
**MAX4113/MAX4118/MAX4120
SMALL-SIGNAL PULSE RESPONSE
($A_{vCL} = +20$)**



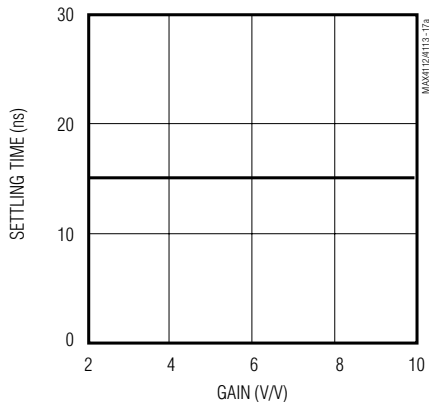
**MAX4113/MAX4118/MAX4120
LARGE-SIGNAL PULSE RESPONSE
($A_{vCL} = +8$)**



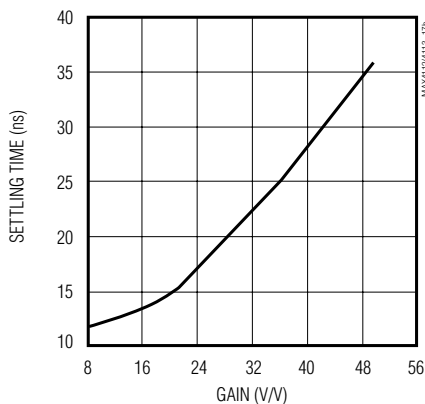
**MAX4113/MAX4118/MAX4120
LARGE-SIGNAL PULSE RESPONSE
($A_{vCL} = +20$)**



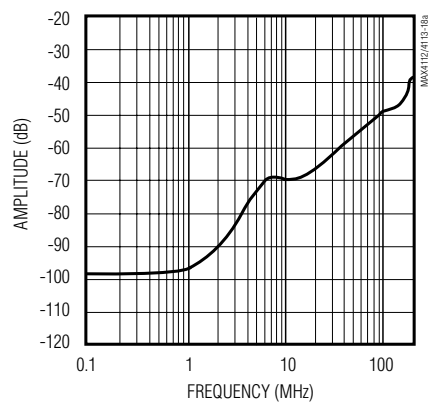
**MAX4112/MAX4117/MAX4119
SETTLING TIME vs. GAIN**



**MAX4113/MAX4118/MAX4120
SETTLING TIME vs. GAIN**



**MAX4117-MAX4120
CROSSTALK vs. FREQUENCY**



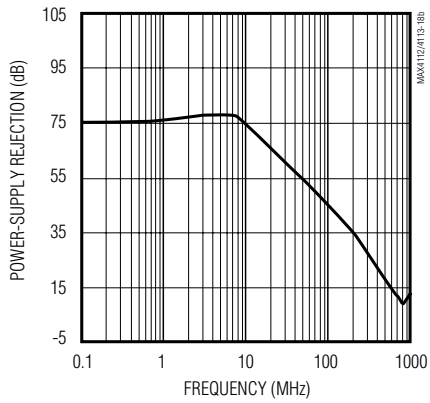
MAX4112/MAX4113/MAX4117-MAX4120

Single/Dual/Quad, 400MHz, Low-Power, Current Feedback Amplifiers

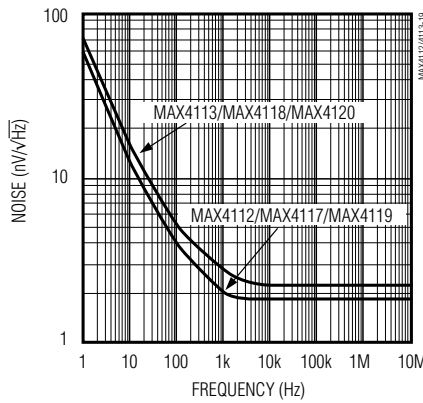
Typical Operating Characteristics (continued)

($V_{CC} = +5V$, $V_{EE} = -5V$, $R_F = 499\Omega$, $R_L = 100\Omega$, $T_A = +25^\circ C$, unless otherwise noted.)

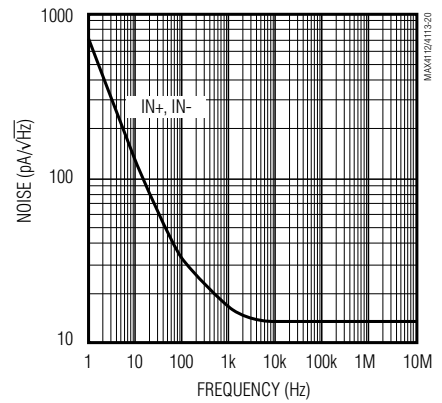
POWER-SUPPLY REJECTION vs. FREQUENCY



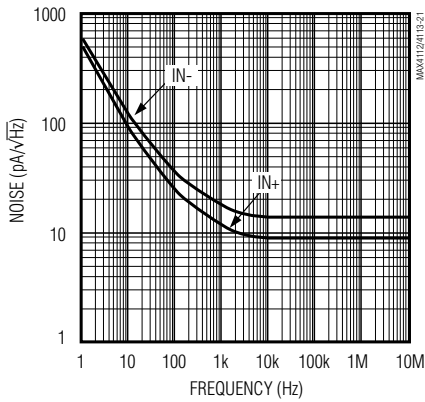
INPUT VOLTAGE NOISE vs. FREQUENCY



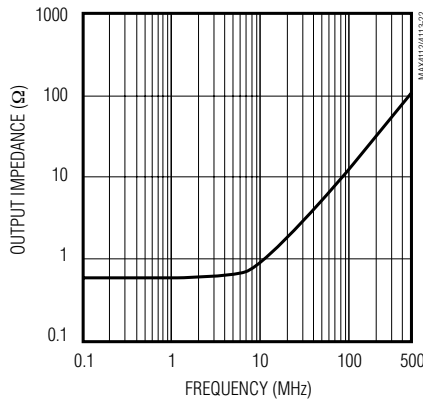
MAX4112/MAX4117/MAX4119 INPUT CURRENT NOISE vs. FREQUENCY



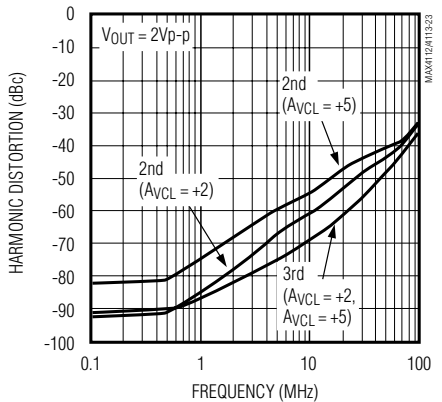
MAX4113/MAX4118/MAX4120 INPUT CURRENT NOISE vs. FREQUENCY



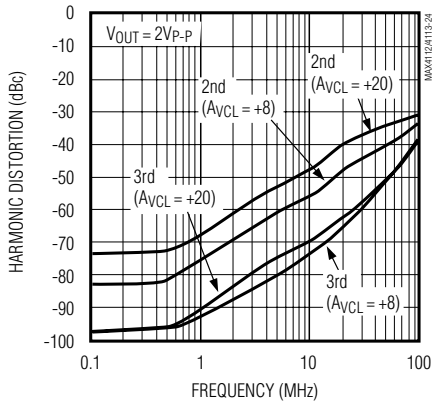
CLOSED-LOOP OUTPUT IMPEDANCE vs. FREQUENCY



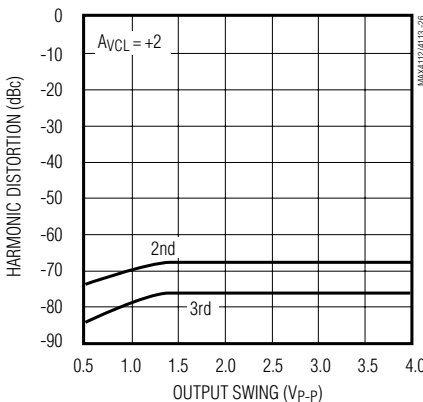
MAX4112/MAX4117/MAX4119 HARMONIC DISTORTION vs. FREQUENCY



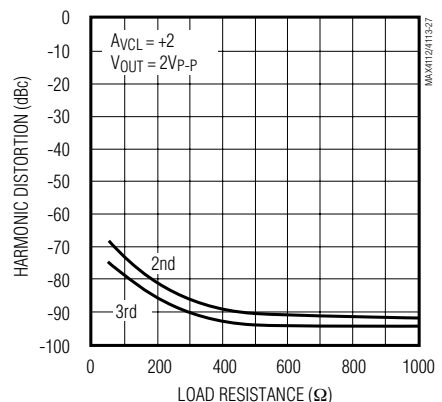
MAX4113/MAX4118/MAX4120 HARMONIC DISTORTION vs. FREQUENCY



MAX4112/MAX4117/MAX4119 5MHz HARMONIC DISTORTION vs. OUTPUT SWING



MAX4112/MAX4117/MAX4119 5MHz HARMONIC DISTORTION vs. LOAD RESISTANCE

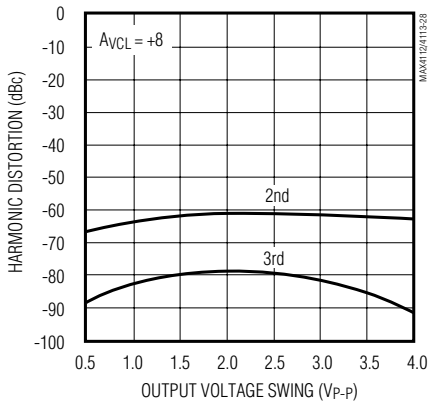


Single/Dual/Quad, 400MHz, Low-Power, Current Feedback Amplifiers

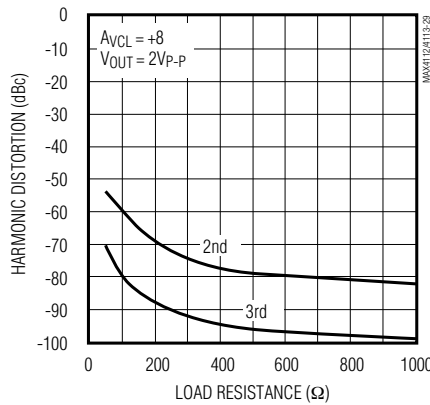
Typical Operating Characteristics (continued)

($V_{CC} = +5V$, $V_{EE} = -5V$, $R_F = 499\Omega$, $R_L = 100\Omega$, $T_A = +25^\circ C$, unless otherwise noted.)

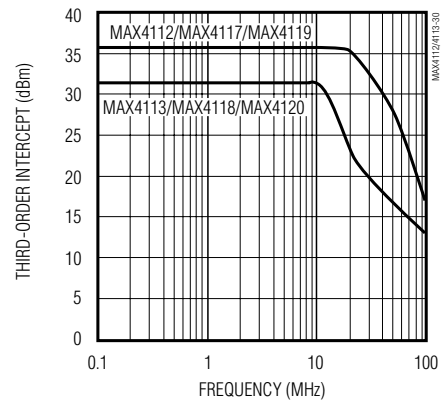
**MAX4113/MAX4118/MAX4120
5MHz HARMONIC DISTORTION
vs. OUTPUT SWING**



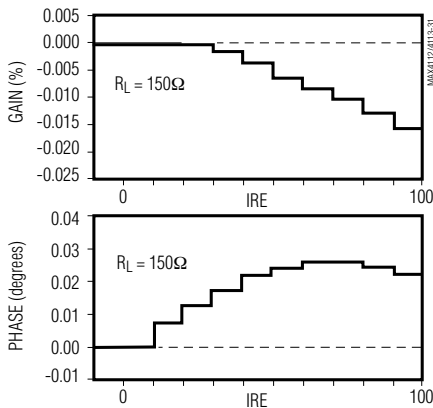
**MAX4113/MAX4118/MAX4120
5MHz HARMONIC DISTORTION
vs. LOAD RESISTANCE**



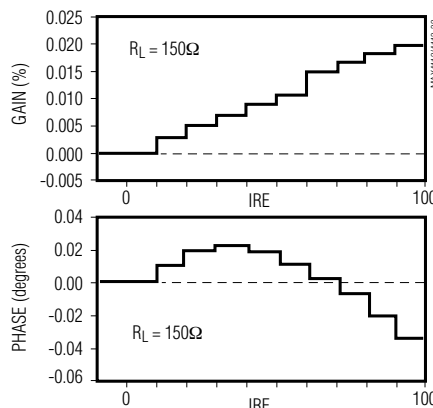
**TWO-TONE THIRD-ORDER INTERCEPT
vs. FREQUENCY**



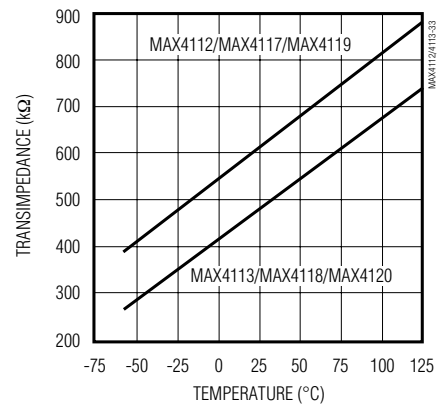
**MAX4112/MAX4117/MAX4119
DIFFERENTIAL GAIN and PHASE**



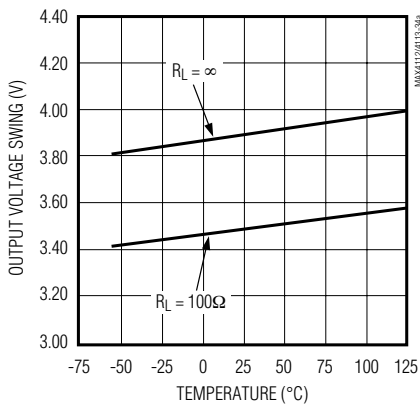
**MAX4113/MAX4118/MAX4120
DIFFERENTIAL GAIN and PHASE**



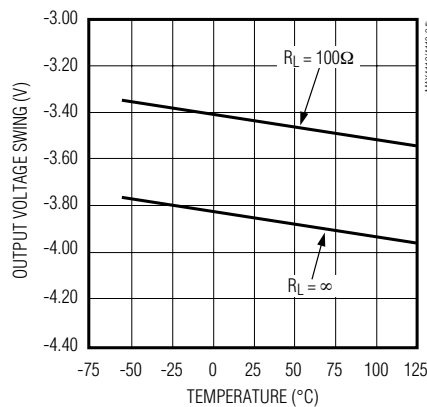
**OPEN-LOOP TRANSIMPEDANCE
vs. TEMPERATURE**



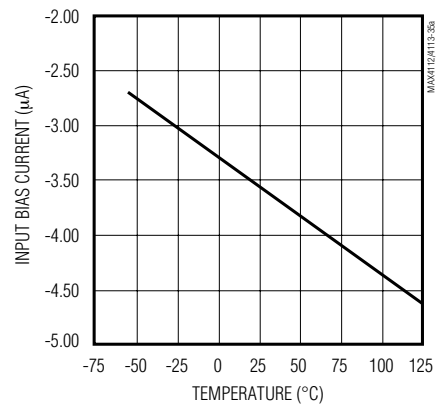
**POSITIVE OUTPUT-VOLTAGE SWING
vs. TEMPERATURE**



**NEGATIVE OUTPUT-VOLTAGE SWING
vs. TEMPERATURE**



**POSITIVE INPUT BIAS CURRENT
vs. TEMPERATURE**

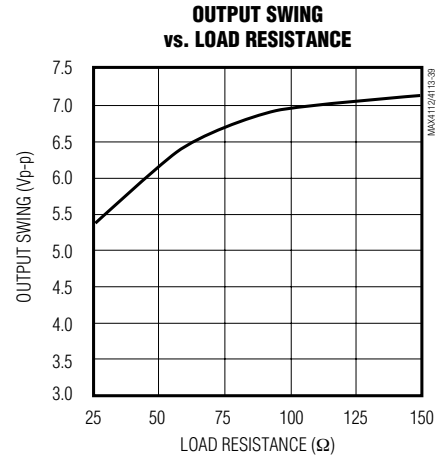
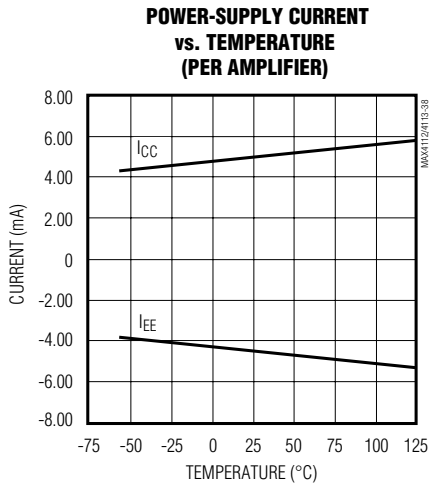
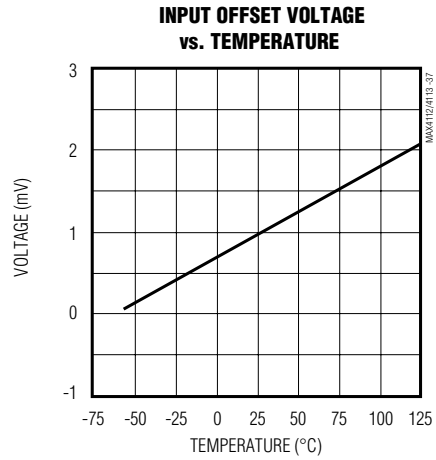
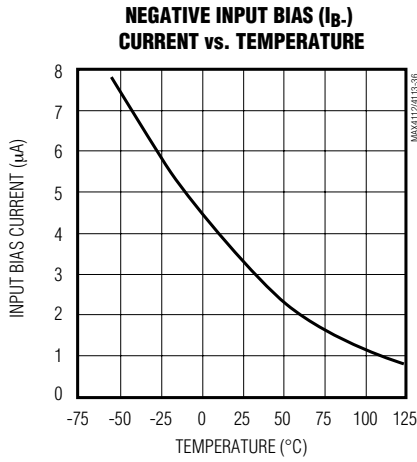


MAX4112/MAX4113/MAX4117-MAX4120

Single/Dual/Quad, 400MHz, Low-Power, Current Feedback Amplifiers

Typical Operating Characteristics (continued)

($V_{CC} = +5V$, $V_{EE} = -5V$, $R_F = 499\Omega$, $R_L = 100\Omega$, $T_A = +25^\circ C$, unless otherwise noted.)



Single/Dual/Quad, 400MHz, Low-Power, Current Feedback Amplifiers

Pin Descriptions

PIN		NAME	FUNCTION
MAX4112 MAX4113 SO/ μ MAX	MAX4117 MAX4118 SO		
1, 5, 8	—	N.C.	No Connection. Not internally connected.
—	1	OUTA	Amplifier A Output
2	—	IN-	Inverting Input
—	2	INA-	Amplifier A Inverting Input
3	—	IN+	Noninverting Input
—	3	INA+	Amplifier A Noninverting Input
4	4	VEE	Negative Power Supply. Connect to -5V.
—	5	INB+	Amplifier B Noninverting Input
6	—	OUT	Amplifier Output
—	6	INB-	Amplifier B Inverting Input
—	7	OUTB	Amplifier B Output
7	8	VCC	Positive Power Supply. Connect to +5V.

PIN		NAME	FUNCTION
MAX4119/MAX4120			
SO	QSOP		
1	1	OUTA	Amplifier A Output
2	2	INA-	Amplifier A Inverting Input
3	3	INA+	Amplifier A Noninverting Input
4	4	VCC	Positive Power Supply. Connect to +5V.
5	5	INB+	Amplifier B Noninverting Input
6	6	INB-	Amplifier B Inverting Input
7	7	OUTB	Amplifier B Output
—	8, 9	N.C.	No Connection. Not internally connected.
8	10	OUTC	Amplifier C Output
9	11	INC-	Amplifier C Inverting Input
10	12	INC+	Amplifier C Noninverting Input
11	13	VEE	Negative Power Supply. Connect to -5V.
12	14	IND+	Amplifier D Noninverting Input
13	15	IND-	Amplifier D Inverting Input
14	16	OUTD	Amplifier D Output

Detailed Description

The MAX4112/MAX4117/MAX4119 are optimized for closed-loop gains (A_{VCL}) of 2V/V or greater, while the MAX4113/MAX4118/MAX4120 are optimized for closed-loop gains of 8V/V or greater. These low-power, high-speed, current feedback amplifiers operate from $\pm 5V$ supplies. They are designed to drive video loads with low distortion characteristics. The MAX4112/MAX4117/MAX4119's differential gain and phase are 0.02% and 0.03°, respectively; the MAX4113/MAX4118/MAX4120 exhibit gain/phase error specifications of 0.02% and 0.04°, respectively. These characteristics, plus a wide 0.1dB gain flatness, make the MAX4112/MAX4113/MAX4117-MAX4120 ideal for use

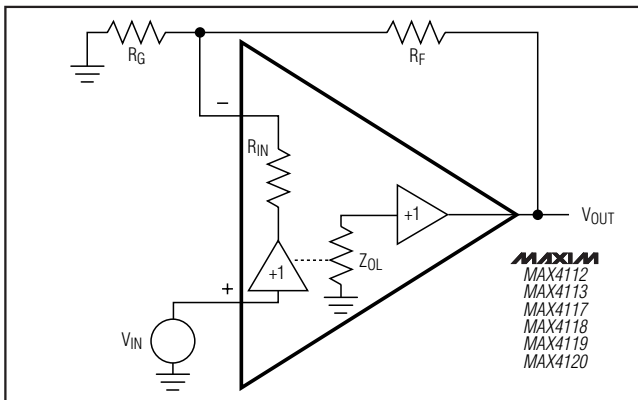


Figure 1. Current Feedback Amplifier

in broadcast and graphics video systems. The combination of ultra-high speed and low power makes these parts suitable for use in general-purpose, high-speed applications, such as medical imaging, industrial instrumentation, and communications systems.

Applications Information

Theory of Operation

Since these devices are current-feedback amplifiers, their open-loop transfer function is expressed as a transimpedance, $\Delta V_{OUT}/\Delta I_{IN}$, or Z_{OL} . The frequency behavior of the open-loop transimpedance is similar to the open-loop gain of a voltage feedback amplifier. That is, it has a large DC value and decreases at approximately 6dB per octave.

Analyzing the follower with gain, as shown in Figure 1, yields the following transfer function:

$$\frac{V_{OUT}}{V_{IN}} = G \times \frac{Z_{OL}(s)}{Z_{OL}(s) + G \times (R_{IN} + R_F)}$$

where $G = A_{VCL} = 1 + (R_F / R_G)$, and $R_{IN} = 1 / g_M \approx 30\Omega$.

Single/Dual/Quad, 400MHz, Low-Power, Current Feedback Amplifiers

At low gains, $G \times R_{IN} \ll R_F$. Therefore, the closed-loop bandwidth is essentially independent of closed-loop gain. Similarly, $Z_{OL} \gg R_F$ at low frequencies, so that:

$$\frac{V_{OUT}}{V_{IN}} = G = 1 + (R_F / R_G)$$

Layout and Power-Supply Bypassing

The MAX4112/MAX4113/MAX4117-MAX4120 have an RF bandwidth and consequently require careful board layout, including the possible use of constant-impedance microstrip or stripline techniques.

To realize the full AC performance of these high-speed amplifiers, pay careful attention to power-supply bypassing and board layout. The PCB should have at least two layers: a signal and power layer on one side, and a large, low-impedance ground plane on the other side. The ground plane should be as free of voids as possible. With multilayer boards, locate the ground plane on a layer that incorporates no signal or power traces.

Regardless of whether a constant-impedance board is used, observe the following guidelines when designing the board. Wire-wrapped boards are much too inductive, and breadboards are much too capacitive; neither should be used. IC sockets increase parasitic capacitance and inductance, and should not be used. In general, surface-mount components give better high-frequency performance than through-hole components. They have shorter leads and lower parasitic reactances. Keep lines as short and as straight as possible. Do not make 90° turns; round all corners.

Observe high-frequency bypassing techniques to maintain the amplifier's accuracy. The bypass capacitors should include a 1000pF ceramic capacitor between each supply pin and the ground plane, located as close to the package as possible. Next, place a

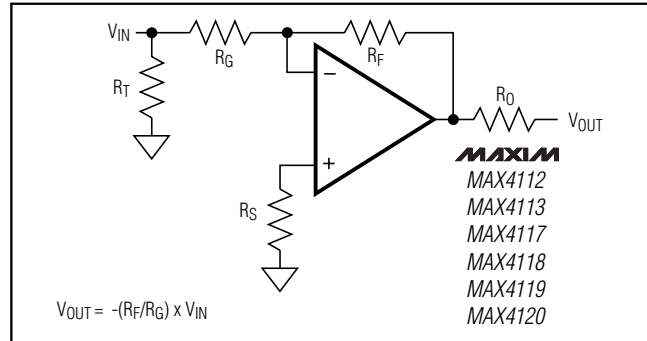


Figure 2a. Inverting Gain Configuration

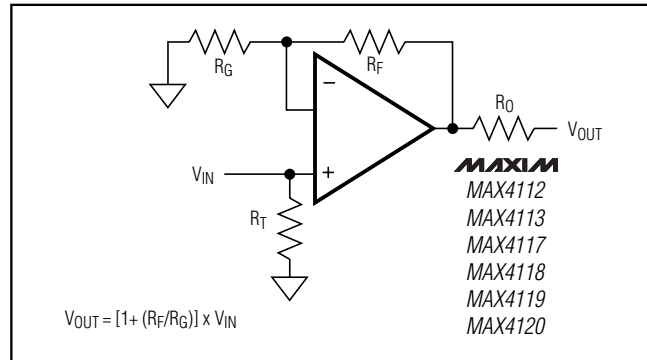


Figure 2b. Noninverting Gain Configuration

0.01μF to 0.1μF ceramic capacitor in parallel with each 1000pF capacitor, and as close to them as possible. Then place a 10μF to 15μF low-ESR tantalum at the point of entry (to the PCB) of the power-supply pins. The power-supply trace should lead directly from the tantalum capacitor to the VCC and VEE pins. To minimize parasitic inductance, keep PC traces short and use surface-mount components.

Table 1. Recommended Component Values

COMPONENT	AvCL = +2			AvCL = +8		
	MAX4112	MAX4117	MAX4119	MAX4113	MAX4118	MAX4120
R _F (Ω)	600	600	500	500	330	330
R _G (Ω)	600	600	500	69	47	47
R _O (Ω)	49.9	49.9	49.9	49.9	49.9	49.9
R _T (Ω)	49.9	49.9	49.9	49.9	49.9	49.9
-3dB Small-Signal Bandwidth (MHz)	400	400	270	270	300	300
0.1dB Gain Flatness (MHz)	100	100	100	115	115	115
Large-Signal Bandwidth (MHz)	280	280	145	240	240	240

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MAX4112/MAX4113/MAX4117-MAX4120

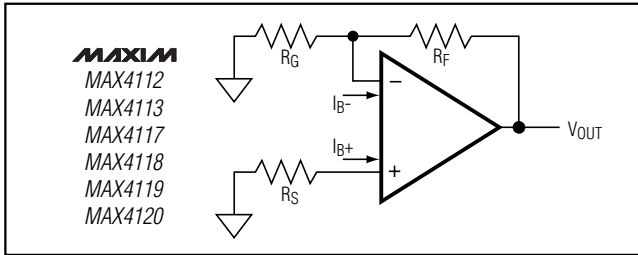


Figure 3. Output Offset Voltage

Choosing Feedback and Gain Resistors

The MAX4112/MAX4113/MAX4117–MAX4120 are current feedback amplifiers. Increasing feedback resistor values will decrease peaking. Use the input resistor (R_G) to change the standard inverting and noninverting configurations. Notice that the gain of the noninverting circuit (Figure 2b) is 1 plus the magnitude of the inverting closed-loop gain (Table 1).

DC and Noise Errors

There are several major error sources to consider in any operational amplifier. These apply equally to the MAX4112/MAX4113/MAX4117–MAX4120. Offset-error terms are given by the equation below. Voltage and current-noise errors are root-square summed and therefore computed separately. In Figure 3, the total output offset voltage is determined by:

- The input offset voltage (V_{OS}) times the closed-loop gain ($1 + (R_F / R_G)$).
- The positive input bias current (I_{B+}) times the source resistor (R_S) (usually 50Ω or 75Ω), plus the negative input bias current (I_{B-}) times the parallel combination of R_G and R_F . In current-mode feedback amplifiers, the input bias currents may flow into or out of the device. For this reason, there is no benefit to matching the resistance at both inputs.

The equation for total DC error is:

$$V_{OUT} = \left[(I_{B+})R_S + (I_{B-})(R_F \parallel R_G) + V_{OS} \right] \left(1 + \frac{R_F}{R_G} \right)$$

- The total output-referred noise voltage is:

$$e_{n(OUT)} = \left(1 + \frac{R_F}{R_G} \right) \sqrt{[(i_{n+})R_S]^2 + [(i_{n-})R_F \parallel R_G]^2 + (e_n)^2}$$

The MAX4112/MAX4117/MAX4119 have a very low, $2nV/\sqrt{Hz}$ noise voltage. The current noise at the positive input (i_{n+}) is $13pA/\sqrt{Hz}$, and the current noise at the inverting input (i_{n-}) is $14pA/\sqrt{Hz}$.

An example of the DC error calculations, using the MAX4112 typical data and the typical operating circuit where $R_F = R_G = 600\Omega$ ($R_F \parallel R_G = 300\Omega$) and $R_S = 50\Omega$, gives the following:

$$V_{OUT} = (3.5 \times 10^{-6} \times 50 + 3.5 \times 10^{-6} \times 300 + 10^{-3}) (1 + 1)$$

$$V_{OUT} = 4.45mV$$

Calculating total output noise in a similar manner yields:

$$e_{n(OUT)} = (1 + 1) \sqrt{(13 \times 10^{-12} \times 50)^2 + (14 \times 10^{-12} \times 300)^2 + (2 \times 10^{-9})^2}$$

$$e_{n(OUT)} = 9.4nV/\sqrt{Hz}$$

With a 200MHz system bandwidth, this calculates to $133\mu V_{RMS}$ (approximately $797\mu V_{P-P}$, choosing the six-sigma value).

Resistor Types

Surface-mount resistors are the best choice for high-frequency circuits. They are of similar material to metal-film resistors, but are deposited using a thick-film process in a flat, linear manner that minimizes inductance. Their small size and lack of leads also minimizes parasitic inductance and capacitance, yielding more predictable performance.

Metal-film resistors with leads are manufactured using a thin-film process where resistive material is deposited in a spiral layer around a ceramic rod. Although the materials used are noninductive, the spiral winding presents a small inductance (about 5nH) that may have an adverse effect on high-frequency circuits.

Carbon-composition resistors with leads are manufactured by pouring the resistor material into a mold. This process yields relatively low-inductance resistors that are very useful in high-frequency applications, although they tend to cost more and have more thermal noise than other types. The ability of carbon-composition resistors to self-heal after a large current overload makes them useful in high-power RF applications.

For general-purpose use, surface-mount metal-film resistors seem to have the best overall performance for low cost, low inductance, and low noise.

Video Line Driver

The MAX4112/MAX4113/MAX4117–MAX4120 are optimized (gain flatness) to drive coaxial transmission lines when the cable is terminated at both ends, as shown in Figure 4. Cable frequency response can cause variations in the flatness of the signal.

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Driving Capacitive Loads

The MAX4112/MAX4113/MAX4117-MAX4120 are optimized for AC performance. They are not designed to drive highly capacitive loads. Reactive loads decrease phase margin and can produce excessive ringing and oscillation. Figure 5a shows a circuit that eliminates this problem. The small (usually 5Ω to 22Ω) isolation resistor, R_S , placed before the reactive load prevents ringing and oscillation. At higher capacitive loads, AC performance is controlled by the interaction of the load capacitance and isolation resistor.

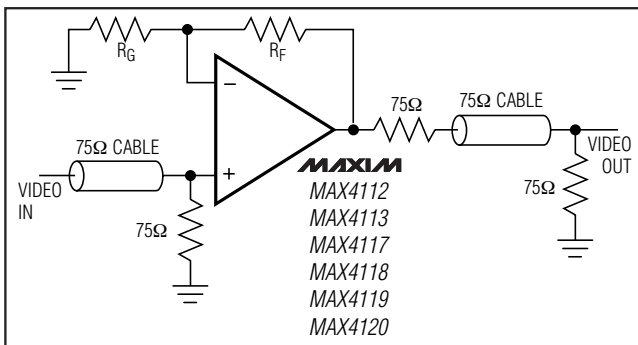


Figure 4. Video Line Driver

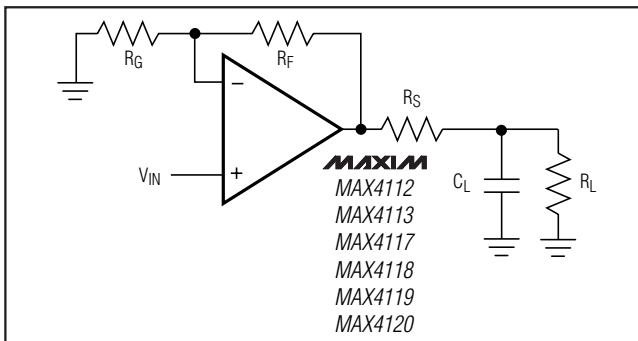


Figure 5a. Using an Isolation Resistor (R_S) for High Capacitive Loads

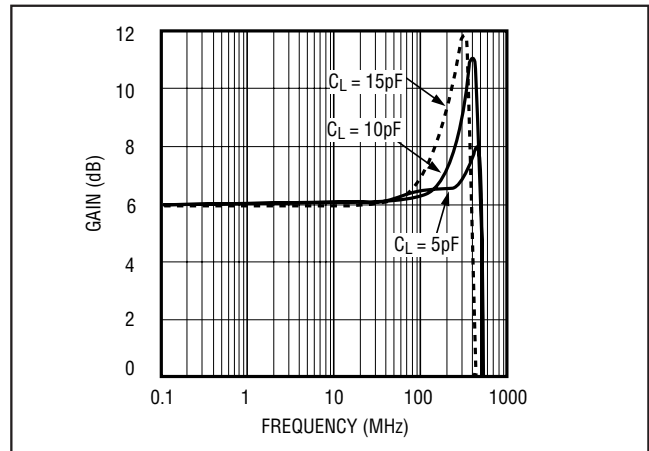


Figure 5b. Frequency Response vs. Capacitive Load—No Isolation Resistor

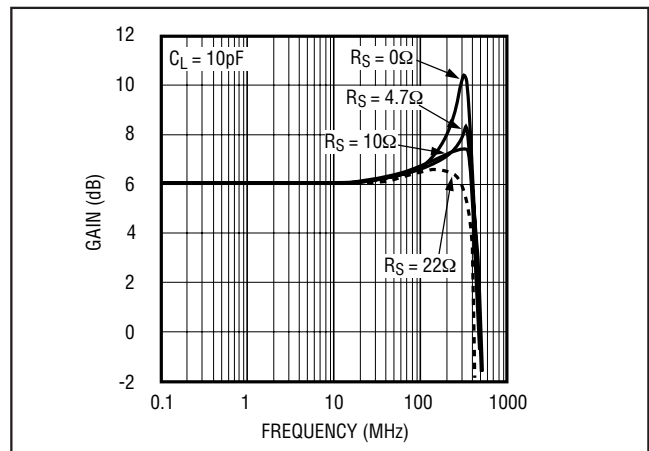


Figure 5c. Frequency Response vs. Isolation Resistance (see Figure 5a for circuit)

Ordering Information (continued)

PART	TEMP RANGE	PIN-PACKAGE	PKG CODE
MAX4119ESD	-40°C to +85°C	14 SO	S14-1
MAX4119EEE	-40°C to +85°C	16 QSOP	E16-1
MAX4120ESD	-40°C to +85°C	14 SO	S14-1
MAX4120EEE	-40°C to +85°C	16 QSOP	E16-1

*Contact factory for QSOP package availability.

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Chip Information

TRANSISTOR COUNT: 53 (MAX4112/MAX4113)
112 (MAX4117/MAX4118)
220 (MAX4119/MAX4120)

SUBSTRATE CONNECTED TO V_{EE}

Revision History

Pages changed at Rev 3: 1–3, 6, 7, 10–12

Mouser Electronics

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