### **ABSOLUTE MAXIMUM RATINGS**





**Note 1:** Package thermal resistances were obtained using the method described in JEDEC specification JESD51-7, using a fourlayer board. For detailed information on package thermal comsiderations, refer to **www.maxim-ic.com/thermal-tutorial**.

*Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.*

### **ELECTRICAL CHARACTERISTICS**

(V<sub>IN</sub> = +12V, V<sub>OUT</sub> = 6V, Circuit of Figure 1, T<sub>A</sub> = 0°C to +85°C, unless otherwise noted. Typical values are at T<sub>A</sub> = +25°C.)



### **ELECTRICAL CHARACTERISTICS (continued)**

(V<sub>IN</sub> = +12V, V<sub>OUT</sub> = 6V, Circuit of Figure 1, T<sub>A</sub> = 0°C to +85°C, unless otherwise noted. Typical values are at T<sub>A</sub> = +25°C.)



## **ELECTRICAL CHARACTERISTICS**

( $V_{IN}$  = +12V,  $V_{OUT}$  = 6V, Circuit of Figure 1, T<sub>A</sub> = -40°C to +85°C, unless otherwise noted.)



**Note 2:** This ratio is generated by a 1:8 clock divider and is not an error source for current calculations.

(Circuit of Figure 1,  $T_A = +25^{\circ}C$ , unless otherwise noted.)





**MAX1640**

### 1.490 1.500 1.510 **MAX1640 OUTPUT CURRENT vs. OUTPUT VOLTAGE** MAX1640/41-TOC03 OUTPUT CURRENT (A)  $40^{\circ}$ C  $T_A = +85^{\circ}$ C

*\_Typical Operating Characteristics*







**MAX1641**

**QUIESCENT CURRENT vs. INPUT VOLTAGE (NO-LOAD)**











#### **LINE-TRANSIENT RESPONSE**



4 Maxim Integrated

### *\_Typical Operating Characteristics (continued)*

(Circuit of Figure 1,  $T_A = +25^{\circ}$ C, unless otherwise noted.)



A: OUTPUT CURRENT, D0 = D1 = 0 1A/div B: LOAD VOLTAGE, AC coupled, 500mV/div



B: OUTPUT CURRENT, 0.5A/div

### *\_Pin Description*



*\_ Functional Diagram*





*Figure 1a. Standard Application Circuit Figure 1b. Standard Application Circuit*

### *\_\_\_\_\_\_\_\_\_\_\_\_\_\_\_Detailed Description*

The MAX1640/MAX1641 switch-mode current sources utilize a hysteretic, current-mode, step-down pulsewidth-modulation (PWM) topology with constant offtime. Internal comparators control the switching mechanism. These comparators monitor the current through a sense resistor (R<sub>SENSE</sub>) and the voltage at TERM. When inductor current reaches the current limit  $[(VCS<sub>+</sub> - VCS<sub>-</sub>) / RSENSE]$ , the P-channel FET turns off and the N-channel FET synchronous rectifier turns on. Inductor energy is delivered to the load as the current ramps down. This ramp rate depends on  $R_{TOFF}$  and inductor values. When off-time expires, the P-channel FET turns back on and the N-channel FET turns off.

Two digital inputs, D0 and D1, select between four possible current levels (Table 1). In pulse-trickle mode, the



part operates for 12.5% of the period set by R<sub>TOFF</sub>, resulting in a lower current for pulse-trickle charging. See the *Functional Diagram*. Figures 1a and 1b show the standard application circuits.

#### *Charge Mode: Programming the Output Currents*

The sense resistor, RSENSE, sets two charging current levels. Choose between these two levels by holding D0 high, and toggling D1 either high or low (Table 1). The fast-charge current level equals V<sub>CS</sub> / R<sub>SENSE</sub> where V<sub>CS</sub> is the full-scale current-sense voltage of 150mV. Alternatively, calculate this current by VREF / (13.3RSENSE). The top-off current equals VSET / (13.3RSENSE). A resistor-divider from REF to GND programs the voltage at SET (Figure 2).

The voltage at SET is given by:

 $R1 = R2$  (V<sub>REF</sub> / V<sub>SET</sub> -1);  $10kΩ < R2 < 300kΩ$ 

where  $V_{REF}$  = 2V and  $V_{SET}$  is proportional to the desired output current level.











*Figure 3a. Setting the Maximum Output Voltage Level*



*Figure 3b. Setting the Maximum Output Voltage Level*

The MAX1640/MAX1641 are specified for VSET between OV and  $V_{REF}$ . For  $V_{SET} > V_{REF}$ , output current increases linearly (with reduced accuracy) until it clamps at  $V<sub>SET</sub> \approx 4V$ .

#### *Pulse-Trickle Mode: Selecting the Pulse-Trickle Current*

Pulling D0 low and D1 high selects pulse-trickle mode. This current equals  $V_{\text{SET}}$  / (13.3R $_{\text{SENSE}}$ ) and remains on for 12.5% of the period set by RTOFF. Pulse-trickle current maintains full charge across the battery and can slowly charge a cold battery before fast charging commences.

$$
PERIOD = 3.2 \times 10^{-7} \times R_{TOFF} (sec)
$$

### *Off Mode: Turning Off the Output Current*

Pulling D0 and D1 low turns off the P-channel FET and hence the output current flow. This mode also controls end of charge and protects the battery against excessive temperatures.

#### *Setting the Maximum Output Voltage Level*

The maximum output voltage should be programmed to a level higher than the output/battery voltage (ILOAD x RLOAD). An external resistor-divider between the output and ground (Figure 3) sets the voltage at TERM. Once the voltage at TERM exceeds the reference, the internal comparator turns off the P-channel FET, terminating current flow. Select R4 in the 10kΩ to 500kΩ range. R3 is given by:

$$
R3 = R4 ((VOUT / VTERM) - 1)
$$

where  $V$ TERM = 2V and  $V_{\text{OUT}}$  is the desired output voltage.

#### *Programming the Off-Time*

When programming the off-time, consider such factors as maximum inductor current ripple, maximum output voltage, inductor value, and inductor current rating. The output current ripple is less than the inductor current ripple and depends heavily on the output capacitor's size.

Perform the following steps to program the off-time:

- 1) Select the maximum output current ripple. IR(A)
- 2) Select the maximum output voltage.  $V_{\text{OUT}}(MAX)(V)$
- 3) Calculate the inductor value range as follows:

 $L_{MIN} = (V_{OUTMAX} \times 1 \mu s) / I_R$ 

 $L_{MAX} = (V_{OUTMAX} \times 10 \mu s) / I_R$ 

- 4) Select an inductor value in this range.
- 5) Calculate t<sub>OFF</sub> as follows:

$$
t_{\text{OFF}} = \frac{L \times I_{\text{R}}}{V_{\text{OUTMAX}}}
$$

6) Program tOFF by selecting RTOFF from:

 $RTOFF = (29.3 \times 10^9) \times 10^{6}$ 

7) Calculate the switching frequency by:

$$
fs = 1 / (ton + toFF)
$$

where  $t_{ON} = (I_R \times L) / (V_{IN} - V_{OUT})$  and  $I_R = (V_{OUT} \times I_R)$ to  $F$ ) / L. L is the inductor value,  $V_{IN}$  is the input voltage,  $V_{\text{OUT}}$  is the output voltage, and  $I_R$  is the output peak-to-peak current ripple.

Note that R<sub>TOFF</sub> sets both the off-time and the pulsetrickle charge period.

#### *Reference*

The on-chip reference is laser trimmed for a precise 2V at REF. REF can source no more than 50µA. Bypass REF with a 0.1µF capacitor to ground.

#### *Constant-Current Loop: AC Loop Compensation*

The constant-current loop's output is brought out at CC. To reduce noise due to variations in switching currents, bypass CC with a 1nF to 100nF capacitor to ground. A large capacitor value maintains a constant average output current but slows the loop response to changes in switching current. A small capacitor value speeds up the loop response to changes in switching current,

generating increased ripple at the output. Select C<sub>CC</sub> to optimize the ripple vs. loop response.

#### *Synchronous Rectification*

Synchronous rectification reduces conduction losses in the rectifier by shunting the Schottky diode with a lowresistance MOSFET switch. In turn, efficiency increases by about 3% to 5% at heavy loads. To prevent crossconduction or "shoot-through," the synchronous rectifier turns on shortly after the P-channel power MOSFET





turns off. The synchronous rectifier remains off for 90% of the off-time. In low-cost designs, the synchronous rectifier FET may be replaced by a Schottky diode.

### *Component Selection*

#### *External Switching Transistors*

The MAX1640/MAX1641 drive an enhancement-mode P-channel MOSFET and a synchronous-rectifier Nchannel MOSFET (Table 2).

When selecting a P-channel FET, some important parameters to consider are on-resistance (rDS(ON)), maximum drain-to-source voltage (V<sub>DS</sub> max), maximum gate-to-source voltage (VGS max), and minimum threshold voltage (V<sub>TH</sub> min).

In high-current applications, MOSFET package power dissipation often becomes a dominant design factor. I2R power losses are the greatest heat contributor for both high-side and low-side MOSFETs. Switching losses affect the upper MOSFET only (P-channel), since the Schottky rectifier or the N-FET body diode clamps the switching node before the synchronous rectifier turns on.



*Figure 4. Microcontroller Battery Charger*

#### *Rectifier Diode*

If an N-channel MOSFET synchronous rectifier is not used, a Schottky rectifier is needed. The MAX1640/ MAX1641's high switching frequency demands a highspeed rectifier (Table 2). Schottky diodes such as the 1N5817–1N5822 are recommended. Make sure the Schottky diode's average current rating exceeds the peak current limit and that its breakdown voltage exceeds the output voltage (VOUT). For high-temperature applications, Schottky diodes may be inadequate due to their high leakage current; high-speed silicon diodes such as the MUR105 or EC11FS1 can be used instead. At heavy loads and high temperatures, the benefits of a Schottky diode's low forward voltage may outweigh the disadvantage of high leakage current. If the application uses an N-channel MOSFET synchronous rectifier, a parallel Schottky diode is usually unnecessary except with very high charge current  $(> 3$ amps). Best efficiency is achieved with both an N-channel MOSFET and a Schottky diode.

#### *Inductor Value*

Refer to the section *Programming the Off-Time* to select the proper inductor value. There is a trade-off between inductor value, off-time, output current ripple, and switching frequency.

### *\_\_\_\_\_\_\_\_\_\_Applications Information*

#### *All-Purpose Microcontroller Battery Charger: NiCd, NiMH*

In applications where a microcontroller is available, the MAX1640/MAX1641 can be used as a low-cost battery charger (Figure 4). The controller takes over fast charge, pulse-trickle charge, charge termination, and other smart functions. By monitoring the output voltage at  $V_{\text{OUT}}$ , the controller initiates fast charge (set D0 and D1 high), terminates fast charge and initiates top-off (set D0 high and D1 low), enters trickle charge (set D0 low and D1 high), or shuts off and terminates current flow (set D0 and D1 low).

#### *Layout and Grounding*

Due to high current levels and fast switching waveforms, proper PC board layout is essential. High-current ground paths should be connected in a star configuration to PGND. These traces should be wide to

reduce resistance and as short as possible to reduce stray inductance. All low-current ground paths should be connected to GND. Place the input bypass capacitor as close as possible to IN. See the MAX1640 EV kit for layout example.

### *\_\_\_\_\_\_\_\_\_\_\_\_\_\_\_\_\_\_\_Chip Information*

PROCESS: BiCMOS

### *Package Information*

(For the latest package outline information and land patterns, go to www.maxim-ic.com/packages. Note that a "+", "#", or "-" in the package code indicates RoHS status only. Package drawings may show a different suffix character, but the drawing pertains to the package regardless of RoHS status.package drawing(s) in this data sheet may not reflect the most current specifications. For the latest package outline information, go to **www.maxim-ic.com/packages**.)



## *\_Revision History*





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