### **ABSOLUTE MAXIMUM RATINGS**





Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

### **ELECTRICAL CHARACTERISTICS**

(V<sub>CC</sub> = 5V, V<sub>EE</sub> = -5V, T<sub>A</sub> = T<sub>MIN</sub> to T<sub>MAX</sub>, unless otherwise noted. Typical values are at T<sub>A</sub> = +25°C.)



### **ELECTRICAL CHARACTERISTICS (continued)**

(V<sub>CC</sub> = 5V, V<sub>EE</sub> = -5V, T<sub>A</sub> = T<sub>MIN</sub> to T<sub>MAX</sub>, unless otherwise noted. Typical values are at T<sub>A</sub> = +25°C.)



( $V_{CC}$  = 5V,  $V_{EE}$  = -5V,  $T_A$  = +25°C, unless otherwise noted.)

### **\_Typical Operating Characteristics**



*IVI A* XI*IV*I



MAX4100/MAX4101 **MAX4100/MAX4101**

### **\_Typical Operating Characteristics (continued)**

( $V_{CC}$  = 5V,  $V_{EE}$  = -5V,  $T_A$  = +25°C, unless otherwise noted.)



**MAX4100/MAX4101 101bXA100/MAXA101** 



**MAXM** 

**6 \_**

### **\_Typical Operating Characteristics (continued)**

( $V_{CC}$  = 5V,  $V_{EE}$  = -5V,  $T_A$  = +25°C, unless otherwise noted.)



**MAX4100 DIFFERENTIAL GAIN AND PHASE**





**MAX4101 DIFFERENTIAL GAIN AND PHASE**



**\_Pin Description**



**MAXIM** 

**MAX4100/MAX4101** are low-power, high-bandwidt operational amplifiers optimized for driving back-term nated cables in composite video, RGB, and RF systems The MAX4100 is unity-gain stable, and the MAX4101 is optimized for The MAX4100/MAX4101 are low-power, high-bandwidth operational amplifiers optimized for driving back-terminated cables in composite video, RGB, and RF systems. The MAX4100 is unity-gain stable, and the MAX4101 is optimized for closed-loop gains greater than or equal to  $2$ V/V (A<sub>VCL</sub>  $\geq$  2V/V). While consuming only 5mA (6mA max) supply current, both devices can drive 50Ω backterminated cables to  $\pm 3.1V$  minimum.

The MAX4100 features a bandwidth in excess of 500MHz and a 0.1dB gain flatness of 65MHz. It offers differential gain and phase errors of 0.06%/0.04°, respectively. The MAX4101 features a -3dB bandwidth of 200MHz, a 0.1dB bandwidth of 50MHz, and 0.07%/0.04° differential gain and phase.

Available in small 8-pin SO and µMAX packages, these ICs are ideally suited for use in portable systems (in RGB, broadcast, or consumer video applications) that benefit from low power consumption.

### **\_\_\_\_\_\_\_\_\_\_Applications Information**

#### **Layout and Power-Supply Bypassing**

The MAX4100/MAX4101 have an RF bandwidth and, consequently, require careful board layout. Depending on the size of the PC board used and the frequency of operation, it may be desirable to use constant-impedance microstrip or stripline techniques.

To realize the full AC performance of this high-speed amplifier, pay careful attention to power-supply bypassing and board layout. The PC board should have at least two layers: a signal and power layer on one side, and a large, low-impedance ground plane on the other side. The ground plane should be as free of voids as possible. With multilayer boards, locate the ground plane on a layer that incorporates no signal or power traces.





Regardless of whether a constant-impedance board is used, it is best to observe the following guidelines when designing the board. Wire-wrap boards are much too inductive, and breadboards are much too capacitive; neither should be used. IC sockets increase parasitic capacitance and inductance, and should not be used. In general, surface-mount components give better high-frequency performance than through-hole components. They have shorter leads and lower parasitic reactances. Keep lines as short and as straight as possible. Do not make 90° turns; round all corners.

High-frequency bypassing techniques must be observed to maintain the amplifier accuracy. The bypass capacitors should include a 1000pF ceramic capacitor between each supply pin and the ground plane, located as close to the package as possible. Next, place a 0.01µF to 0.1µF ceramic capacitor in parallel with each 1000pF capacitor, and as close to each as possible. Then place a 10µF to 15µF low-ESR tantalum at the point of entry (to the PC board) of the power-supply pins. The power-supply trace should lead directly from the tantalum capacitor to the  $V_{CC}$  and  $V_{EE}$  pins. To minimize parasitic inductance, keep PC traces short and use surface-mount components.



Figure 1b. Noninverting Gain Configuration



Figure 1a. Inverting Gain Configuration Figure 1c. MAX4100 Unity-Gain Buffer Configuration





Figure 2. Effect of Feedback Resistor Values and Parasitic Capacitance on Bandwidth

#### **Setting Gain**

The MAX4100/MAX4101 are voltage-feedback op amps that can be configured as an inverting or noninverting gain block, as shown in Figures 1a and 1b. The gain is determined by the ratio of two resistors and does not affect amplifier frequency compensation.

In the unity-gain configuration (as shown in Figure 1c), maximum bandwidth and stability is achieved with the MAX4100 when a small feedback resistor is included. This resistor suppresses the negative effects of parasitic inductance and capacitance. A value of  $24\Omega$  provides the best combination of wide bandwidth, low peaking, and fast settling time. In addition, this resistor reduces the errors from input bias currents.

#### **Choosing Resistor Values**

The values of feedback and input resistors used in the inverting or noninverting gain configurations are not critical (as is the case with current feedback amplifiers). However, take care when selecting because the ohmic values need to be kept small and noninductive for practical reasons.

The input capacitance of the MAX4100/MAX4101 is approximately 2pF. In either the inverting or noninverting configuration, the bandwidth limit caused by the package capacitance and resistor time constant is  $f3dB = 1 / (2\Pi RC)$ , where R is the parallel combination of the input and feedback resistors (RF and RG in Figure 2) and C is the package and board capacitance at the inverting input. Table 1 shows the bandwidth limit for several values of  $RF$  and  $RG$ , assuming  $4pF$  total capacitance (2pF for the MAX4100/MAX4101 and 2pF of PC board parasitics).

### **Table 1. Resistor and Bandwidth Values for Various Gain Configurations**



\* Assuming an infinite bandwidth amplifier.

#### **Resistor Types**

Surface-mount resistors are the best choice for highfrequency circuits. They are of similar material to the metal film resistors, but are deposited using a thick-film process in a flat, linear manner so that inductance is minimized. Their small size and lack of leads also minimize parasitic inductance and capacitance, thereby yielding more predictable performance.

#### **DC and Noise Errors**

There are several major error sources to be considered in any operational amplifier. These apply equally to the MAX4100/MAX4101. Offset-error terms are given by the equation below. Voltage and current noise errors are root-square summed, so are computed separately. Using the circuit in Figure 3, the total output offset voltage is determined by:

- a) The input offset voltage ( $V_{OS}$ ) times the closed-loop gain  $(1 + R_F / R_G)$
- b) The positive input bias current  $(I_{B+})$  times the source resistor  $(R<sub>S</sub>)$  minus the negative input bias current (IB-) times the parallel combination of RG and RF. IOS (offset current) is the difference between the two bias currents. If  $R_G || R_F = R_S$ , this part of the expression becomes IOS x RS.

The equation for total DC error is:

$$
V_{\text{OUT}} = (I_{\text{OS}}R_{\text{S}} + V_{\text{OS}}) \left(1 + \frac{R_{\text{F}}}{R_{\text{G}}}\right)
$$

#### *IVI A* XI*IV*I



Figure 3. Output Offset Voltage

c) Total output-referred noise voltage is shown by the equation below  $(e_n(0UT))$ :

$$
e_{n\text{(OUT)}} = \left(1 + \frac{R_F}{R_G}\right) \sqrt{\left(2i_n R_S\right)^2 + \left(e_N\right)^2}
$$

The MAX4100/MAX4101, with two high-impedance inputs, have low 8nV√Hz voltage noise and only 0.8pA√Hz current noise.

An example of DC error calculations, using the MAX4100/MAX4101 typical data and the typical operating circuit with  $R_F = R_G = 200\Omega$  (Rs = 100 $\Omega$ ), gives:

$$
V_{OUT} = (I_{OS}R_S + V_{OS}) \left(1 + \frac{R_F}{R_G}\right)
$$
  
\n
$$
V_{OUT} = \left(3 \times 10^{-6} \times 10^2 + 1 \times 10^{-3}\right) \left(1 + 1\right)
$$
  
\n
$$
V_{OUT} = 2.6 \text{mV}
$$

Calculating total output-referred noise in a similar manner yields:

$$
e_{n(OUT)} = (1+1)\sqrt{(2 \times 0.8 \times 10^{-12} \times 100)^{2} + (8 \times 10^{-9})^{2}}
$$
  

$$
e_{n(OUT)} = 8nV/\sqrt{Hz}
$$

With a 200MHz system bandwidth, this calculates to 133 $\mu$ V<sub>RMS</sub> (approximately 679 $\mu$ V<sub>p-p</sub>).

In both DC and noise calculations, errors are dominated by offset voltage and noise voltage (rather than by input bias current or noise current).

Metal-film resistors with leads are manufactured using a thin-film process, where resistive material is deposited in a spiral layer around a ceramic rod. Although the materials used are noninductive, the spiral winding presents a small inductance (about 5nH) that may have an adverse effect on high-frequency circuits.



Figure 4a. MAX4100 Bandwidth vs. Capacitive Load



Figure 4b. MAX4100 Bandwidth vs. Capacitive Load and Isolation Resistor



Carbon composition resistors with leads are manufactured by pouring the resistor material into a mold. This process yields a relatively low-inductance resistor that is very useful in high-frequency applications, although they tend to cost more and have more thermal noise than other types. The ability of carbon composition resistors to self-heal after a large current overload makes them useful in high-power RF applications.

For general-purpose use, surface-mount metal-film resistors seem to have the best overall performance for low cost, low inductance, and low noise.

#### **Driving Capacitive Loads**

When driving 50Ω or 75Ω back-terminated transmission lines, capacitive loading is not an issue; therefore an isolation resistor is not required. For other applications where the ability to drive capacitive loads is required, the MAX4100/MAX4101 can typically drive 5pF and 20pF, respectively. Figure 4a illustrates how a capacitive load influences the amplifier's peaking without an isolation resistor (RS). Figure 4b shows how an isolation resistor decreases the amplifier's peaking.

The MAX4100/MAX4101 can drive capacitive loads up to 5pF. By using a small isolation resistor between the amplifier output and the load, large capacitance values may be driven without oscillation (Figure 5a). In most cases, less than  $50\Omega$  is sufficient. Use Figure 5b to determine the value needed in your application. Determine the worst-case maximum capacitive load you may encounter and select the appropriate resistor from the graph.



Figure 5a. Using an Isolation Resistor for High Capacitive Loads (MAX4100)



Figure 5b. Isolation vs. Capacitive Load



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