### High-Accuracy 12-/16-Cell Measurement AFEs

### ABSOLUTE MAXIMUM RATINGS



*Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only, and functional opera*tion of the device at these or any other conditions beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute *maximum rating conditions for extended periods may affect device reliability.*

### PACKAGE THERMAL CHARACTERISTICS (Note 1)



Note 1: Package thermal resistances were obtained using the method described in JEDEC specification JESD51-7, using a four-layer board. For detailed information on package thermal considerations, refer to <www.maximintegrated.com/thermal-tutorial>.

### DC ELECTRICAL CHARACTERISTICS

(Vp = +65V, DGND = AGND, V<sub>L</sub> = V<sub>EN</sub> = +3.3V, V<sub>A</sub> = +5V, C<sub>SAMPLE</sub> = 1µF, T<sub>A</sub> = -40°C to +85°C, unless otherwise noted. Typical values are at  $T_A = +25^{\circ}C$ .) (Note 2)



# High-Accuracy 12-/16-Cell Measurement AFEs

### DC ELECTRICAL CHARACTERISTICS (continued)

( $V_P$  = +65V, DGND = AGND,  $V_L$  =  $V_{EN}$  = +3.3V,  $V_A$  = +5V, C<sub>SAMPLE</sub> = 1µF, T<sub>A</sub> = -40°C to +85°C, unless otherwise noted. Typical values are at  $T_A = +25$ °C.) (Note 2)



# High-Accuracy 12-/16-Cell Measurement AFEs

### DC ELECTRICAL CHARACTERISTICS (continued)

( $V_P$  = +65V, DGND = AGND,  $V_L$  =  $V_{EN}$  = +3.3V,  $V_A$  = +5V, C<sub>SAMPLE</sub> = 1µF, T<sub>A</sub> = -40°C to +85°C, unless otherwise noted. Typical values are at  $T_A = +25$ °C.) (Note 2)



# High-Accuracy 12-/16-Cell Measurement AFEs

### DC ELECTRICAL CHARACTERISTICS (continued)

(V<sub>P</sub> = +65V, DGND = AGND, V<sub>L</sub> = V<sub>EN</sub> = +3.3V, V<sub>A</sub> = +5V, C<sub>SAMPLE</sub> = 1µF, T<sub>A</sub> = -40°C to +85°C, unless otherwise noted. Typical values are at  $T_A = +25$ °C.) (Note 2)



Note 2: All devices are 100% production tested at  $T_A = +25^{\circ}$ C. Limits over the operating temperature range are guaranteed by design. **Note 3:** Where  $n = 1-12$  (MAX14920) and  $n = 1-16$  (MAX14921).

Note 5: Buffer amplifier self-calibrates its offset at power-up and every time it is requested. Due to possible thermal drift after power-up phase, it is suggested to run self-calibration on a regular basis to get best performance (see the *[Buffer Amplifier Offset Calibration](#page-15-0)* section for a detailed explanation).

Note 6: Amplifier error is the sum of all errors including amplifier offset and gain error.

**Note 4:** Output error  $V_{\text{O}}$  ERR is the difference between the input cell difference voltage ( $V_{\text{D}} = V_{\text{C}V(n)} - V_{\text{C}V(n - 1)}$ ) and the output voltage  $\bar{V}_{AOUT}$ . Where n = 1-12 (MAX14920) and n = 1-16 (MAX14921). Output error depends on buffer amplifier errors and parasitic capacitance charge injection error. Since parasitic capacitance error is PCB dependent, output error is guaranteed by design for a sampling capacitor of 1µF and parasitic capacitance less than 2.5pF on CTn (see the *[Measurement Accuracy](#page-14-0)* section for a detailed explanation).

# High-Accuracy 12-/16-Cell Measurement AFEs

### *Timing Diagrams*



*Figure 1. AOUT Delay from SPI Select*







*Figure 3. SPI Timing*

### High-Accuracy 12-/16-Cell Measurement AFEs



### *Typical Operating Characteristics*

 $(V_{C}V_{n} - V_{C}V_{n-1}) = +3.3V$  (where n = 1–12 (MAX14920) and n = 1–16 (MAX14921)),  $T_{A} = +25°C$ , unless otherwise noted.)

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# High-Accuracy 12-/16-Cell Measurement AFEs

### *Pin Configurations*



# High-Accuracy 12-/16-Cell Measurement AFEs

### *Pin Configurations (continued)*



# High-Accuracy 12-/16-Cell Measurement AFEs

### *Pin Description*



# High-Accuracy 12-/16-Cell Measurement AFEs

#### PIN MAX14920 NAME FUNCTION MAX14921 (64 TQFP-EP) (80 TQFP) 21 | 37 | CT11 Sampling Capacitor 11 High Terminal. CT11 internally connects to CV11 when SAMPL is logic-high. Connect a 1µF capacitor between CT11 and CB11. Leave CT11 unconnected if not used. 22 38 CB11 Sampling Capacitor 11 Low Terminal. CB11 internally connects to CV10 when SAMPL is logic-high. Connect a 1µF capacitor between CT11 and CB11. Leave CB11 unconnected if not used. 23 39 CV10 Cell Voltage Input 10. Connect CV10 to cell anode/cathode. Connect CV10 to the highest voltage of the battery cell stack if not used. 24 40 BA10 Cell-Balancing Gate Driver Output 10. Connect BA10 to the gate of the external n-channel FET. Leave BA10 unconnected if not used. 25 41 CT10 Sampling Capacitor 10 High Terminal. CT10 internally connects to CV10 when SAMPL is logic-high. Connect a 1µF capacitor between CT10 and CB10. Leave CT10 unconnected if not used. 26 1 42 CB10 Sampling Capacitor 10 Low Terminal. CB10 internally connects to CV9 when SAMPL is logic-high. Connect a 1µF capacitor between CT10 and CB10. Leave CB10 unconnected if not used. 27 A3 CV9 Cell Voltage Input 9. Connect CV9 to cell anode/cathode. Connect CV9 to the highest voltage of the battery cell stack if not used. 28 44 BA9 Cell-Balancing Gate Driver Output 9. Connect BA9 to the gate of the external n-channel FET. Leave BA9 unconnected if not used. 29 45 CT9 Sampling Capacitor 9 High Terminal. CT9 internally connects to CV9 when SAMPL is logic-high. Connect a 1µF capacitor between CT9 and CB9. Leave CT9 unconnected if not used. 30 46 CB9 Sampling Capacitor 9 Low Terminal. CB9 internally connects to CV8 when SAMPL is logic-high. Connect a 1µF capacitor between CT9 and CB9. Leave CB9 unconnected if not used. 31 47 CV8 Cell Voltage Input 8. Connect CV8 to cell anode/cathode. Connect CV8 to the highest voltage of the battery cell stack if not used. 32 48 BA8 Cell-Balancing Gate Driver Output 8. Connect BA8 to the gate of the external n-channel FET. Leave BA8 unconnected if not used. 33 49 CT8 Sampling Capacitor 8 High Terminal. CT8 internally connects to CV8 when SAMPL is logic-high. Connect a 1µF capacitor between CT8 and CB8. Leave CT8 unconnected if not used. 34 50 CB8 Sampling Capacitor 8 Low Terminal. CB8 internally connects to CV7 when SAMPL is logic-high. Connect a 1µF capacitor between CT8 and CB8. Leave CB8 unconnected if not used. 35  $\bigcup_{\text{CV7}}$  Cell Voltage Input 7. Connect CV7 to cell anode/cathode. Connect CV7 to the highest voltage of the battery cell stack if not used.

# High-Accuracy 12-/16-Cell Measurement AFEs



# High-Accuracy 12-/16-Cell Measurement AFEs



# High-Accuracy 12-/16-Cell Measurement AFEs

#### PIN MAX14920 NAME FUNCTION MAX14921 (64 TQFP-EP) (80 TQFP) — 18 CB16 Sampling Capacitor Connection 16 Low Terminal. CB16 internally connects to CV15 when SAMPL is logic-high. Connect a 1µF capacitor between CT16 and CB16. Leave CB16 unconnected if not used. 19 CV15 CV15 Cell Voltage Input 15. Connect CV15 to cell anode/cathode. Connect CV15 to the highest voltage of the battery cell stack if not used. 20 BA15 Cell-Balancing Gate Driver Output 15. Connect BA15 to the gate of the external n-channel FET. Leave BA15 unconnected if not used. — 21 CT15 Sampling Capacitor Connection 15 High Terminal. CT15 internally connects to CV15 when SAMPL is logic-high. Connect a 1µF capacitor between CT15 and CB15. Leave CT15 unconnected if not used.  $22$  CB15 Sampling Capacitor Connection 15 Low Terminal. CB15 internally connects to CV14 when SAMPL is logic-high. Connect a 1µF capacitor between CT15 and CB15. Leave CB15 unconnected if not used. 23 CV14 Cell Voltage Input 14. Connect CV14 to cell anode/cathode. Connect CV14 to the highest voltage of the battery cell stack if not used. <sup>24</sup> BA14 Cell-Balancing Gate Driver Output 14. Connect BA14 to the gate of the external n-channel FET. Leave BA14 unconnected if not used. — 25 CT14 Sampling Capacitor Connection 14 High Terminal. CT14 internally connects to CV14 when SAMPL is logic-high. Connect a 1µF capacitor between CT14 and CB14. Leave CT14 unconnected if not used. 26 CB14 Sampling Capacitor Connection 14 Low Terminal. CB14 internally connects to CV13 when SAMPL is logic-high. Connect a 1µF capacitor between CT14 and CB14. Leave CB14 unconnected if not used. 27 CV13 Cell Voltage Input 13. Connect CV13 to cell anode/cathode. Connect CV13 to the highest voltage of the battery cell stack if not used. <sup>28</sup> BA13 Cell-Balancing Gate Driver Output 13. Connect BA13 to the gate of the external n-channel FET. Leave BA13 unconnected if not used. — 29 CT13 Sampling Capacitor Connection 13 High Terminal. CT13 internally connects to CV13 when SAMPL is logic-high. Connect a 1uF capacitor between CT13 and CB13. Leave CT13 unconnected if not used. — 30 CB13 Sampling Capacitor Connection 13 Low Terminal. CB13 internally connects to CV12 when SAMPL is logic-high. Connect a 1µF capacitor between CT13 and CB13. Leave CB13 unconnected if not used. — **EP Exposed Pad (MAX14920 Only). Connect EP to AGND.**

### High-Accuracy 12-/16-Cell Measurement AFEs

### *Detailed Description*

The MAX14920/MAX14921 analog front-end devices are used in multicell battery measurement systems to monitor primary/secondary battery packs up to 16 cells/+65V (max). The devices perform the signal conditioning required for enabling accurate cell voltage measurement. Both devices simultaneously sample all cell voltages, allowing accurate state-of-charge and source-resistance determination, even under transient load current conditions. The cell voltage measurements are shifted down to ground reference with unity gain, simplifying external ADC data conversion. The devices enable passive cell balancing through drivers that control external discharge FETs.

A high-accuracy, low-offset amplifier buffers differential voltages up to  $+5V$  for monitoring of the common rechargeable cell technologies such as lithium-ion (Li+). The resulting cell measurement errors from the devices are below  $\pm 0.5$ mV (max). The devices' high accuracy make them ideal for monitoring cell chemistries with very flat discharge curves, such as a lithium-metal phosphate cell. Diagnostics detect open-wire and short conditions, and warn about overvoltage/undervoltage.

The SPI interface is used for control and monitoring through a host controller. The SPI interface is daisychainable. Both devices can operate with a minimum of +6V total stack voltage (typically equating to 3 cells).

#### *Voltage Sampling*

The voltages of all cells are tracked by the sampling capacitors connected between the CTn and CBn pins (where  $n = 1-12$  (MAX14920) and  $n = 1-16$  (MAX14921)), while the **SMPLB** bit is set to 0 and the SAMPL input is driven high [\(Figure 4](#page-13-0)). When the SMPLB bit is set to 1, and the SAMPL input transitions low, all cell voltages are simultaneously sampled on their associated capacitors. The voltages are held by the capacitors while the SMPLB bit is 1, or the SAMPL pin is held low. When sample and holding is controlled by the SAMPL input, set the SMPLB bit to 0. When sample and hold is controlled by the SMPLB bit, keep the SAMPL input high.

In sample phase selecting any cell voltage ( $ECS = 1$ ), AOUT equals  $V<sub>P</sub>/12$  (MAX14920) or  $V<sub>P</sub>/16$  (MAX14921).

Resistors can be placed in series with the CV\_ inputs to filter transients and/or for protection. Consider the switches' on-resistance of  $150\Omega$  (max) when calculating the filter and settling times. In the holding phase, each capacitor's voltage can be independently routed to the analog AOUT output under SPI control.

#### *Voltage Readout*

When the  $\overline{\text{SMPLB}}$  bit is set high, or when the SAMPL input is driven low, the sampling switches are opened after  $0.5\mu s$  (typ) and the cell voltages are held on the external sampling capacitors. Within the time of  $t_{LS}$   $DELAY < 50\mu s$ (max), the capacitors' voltages are all shifted to ground reference. Then the undervoltage/overvoltage monitoring of all cells is valid and the cell voltage is available for sequential readout under SPI control. The SPI control can select the readout of any cell voltages, in any order ([Figure 5](#page-14-1)).

With the ECS bit set to 1, a selected cell's voltage appears at the AOUT output according to the cell selection (as defined by the SC\_ cell select bits). A low-leakage, lownoise, low-offset amplifier buffers the capacitor charge and provides the high-accuracy AOUT analog output. After a settling time of  $t<sub>SFT</sub>$ , from the rising edge of the  $\overline{CS}$  signal, the voltage is available at AOUT with specified accuracy. An ADC can then sample and convert the AOUT voltage. The AOUT output voltage droops over time due to capacitor discharge. The droop time for 1mV of change is larger than t<sub>DROOP</sub> (> C<sub>SAMPLE</sub>/I<sub>CT</sub> LEAK).

<span id="page-13-0"></span>

*Figure 4. Voltage Sampling*

<span id="page-14-1"></span>

### High-Accuracy 12-/16-Cell Measurement AFEs

*Figure 5. SPI Control Cells Voltage Readout*

#### *Measurement Accuracy*

The accuracy of cell voltage monitoring (i.e., the difference of the AOUT voltage relative to the cell voltages) is determined by three factors:

- 1) Held voltage droop due to leakage on the CT\_ pins
- 2) Internal buffer amplifier's voltage errors
- 3) Capacitive level-shifting circuit error

The  $CT$  leakage (1 $\mu$ A, max) is a current that mainly comes from the CV\_ pin and increases with temperature.

Neglecting the PCB leakage across the sampling capacitance, the voltage drift error is given by:

$$
V_{ERR\_LEAK} = \frac{I_{CT\_LEAK}}{C_{SAMPLE}} \times t_{READOUT}
$$

where:

C<sub>SAMPLE</sub> is the sampling capacitance

 $I_{\text{CT}}$  LEAK is the leakage current on the CT\_ pin

 $t_{\text{RFADOUT}}$  is the delay between hold starts and readout of the cell voltage

For example, with  $1\mu$ F sampling capacitors and an ADC conversion rate > 20kHz,  $V_{\text{FRR IFAK}}$  is less than 1mV. Cells with a higher common-mode voltage have a higher leakage. To reduce the voltage drift over time, start sequential voltage readout from the highest cell in the stack first.

<span id="page-14-0"></span>The buffer amplifier errors are nondeterministic in nature, and vary from chip to chip. They are also affected by temperature. The buffer amplifier offset error can be calibrated out through an internal offset-calibration function. This calibration is automatically performed at power-up. The calibration can also be initiated under SPI control. Due to temperature drifts over time, it is best done on a regular basis. Once the buffer amplifier offset is calibrated out, the total error of the buffer is below 0.3mV. After power-up, if the devices do not calibrate regularly, a temperature offset drift of  $\pm 1.5$ µV/°C can occur.

The level shifting is subject to deterministic errors due to charge injection by parasitic PCB-related capacitance on the CT\_ pins. The charge-injected sampling error can be calculated as follows:

$$
V_{ERR\_CHARGE\_INJECTION} = \frac{C_{PAR}}{C_{SAMPLE}} \times V_{CTn} \times \left(\frac{1}{1 - e^{-t_{SAMPLE}}/(2R_{SW} \times C_{SAMPLE})}\right)
$$

where:

CPAR is the parasitic capacitance of the CTn pin, where  $n = 1-12$  (MAX14920) and  $n = 1-16$  (MAX14921) CSAMPLE is the sampling capacitor RSW is the sampling switch resistance  $V_{\text{C}}$ T<sub>n</sub> is the voltage of the CTn pin with respect to AGND, where  $n = 1-12$  (MAX14920) and  $n = 1-16$ (MAX14921)

t<sub>SAMPL</sub> is the sampling time

### High-Accuracy 12-/16-Cell Measurement AFEs

<span id="page-15-1"></span>

*Figure 6. Charge Injection Sampling Error Voltage for 1pF Parasitic Capacitance*

[Figure 6](#page-15-1) shows the charge-injected sampling error for 1pF of parasitic capacitance in worst-case conditions for a 1µF sampling capacitor.

Minimizing the parasitic capacitance on the CT\_ pins to a few picofarads, with a sampling capacitor of  $1\mu$ F, is enough to achieve output error below 1mV target. This error can be further reduced by increasing the sampling capacitor value and consequently increasing the sampling time.

Alternatively, if a sampling capacitor lower than  $1\mu$ F or a parasitic capacitance of more than 15pF are present, these errors can be calibrated out to achieve a < 1mV accuracy level through a calibration procedure for each cell. These per-cell errors are simply subtracted from every cell voltage measurement (see the *[Parasitic Capacitance Charge](#page-15-2) [Injection Error Calibration](#page-15-2)* section).

#### <span id="page-15-2"></span>*Parasitic Capacitance Charge Injection Error Calibration*

This calibration is performed with all cells connected to the CV\_ terminals. Setting the [ECS, SC0, SC1, SC2, SC3] bits to [0, 0, 0, 0, 0] configure the devices for parasitic capacitance charge-injection error calibration.

During the sampling phase, every capacitor's terminals are shorted by an internal calibration sampling switch (RSWCAL =  $800\Omega$  typ), so that only the parasitic capacitance is charged to the cell's common-mode voltage V<sub>CTn</sub>, where  $n = 1-12$  (MAX14920) and  $n = 1-16$ (MAX14921).

The subsequent cell voltage readout sequence then shows the value of VERR\_CHARGE\_INJECTION for

each of the 12/16 cells at AOUT, multiplied by 128. If VERR\_CHARGE\_INJECTION is large enough to affect the required 1mV accuracy, this calibration method provides a measurement of the parasitic capacitance on each CT pin so the microcontroller can use this to correct VERR\_INJECTION in its readings.

Different correction algorithms are possible for the microcontroller using the calibration readout voltages. A simple way to correct cell voltages is to store the ADC data of each cell obtained during calibration (i.e., error values), divided by 128, and subtract these from the subsequently measured cell voltages.

#### <span id="page-15-0"></span>*Buffer Amplifier Offset Calibration*

On power-up, the devices automatically go through a self-calibration phase to minimize the internal buffer's offset voltage. In addition, the offset voltage can be calibrated out at any time under host control. Offset calibration is configurable by setting the [ECS, SC0, SC1, SC2, SC3] bits to [0, 1, 0, 0] and is initiated on the low to high CS transition in sampling phase. This offset-calibration procedure takes 8ms to complete. The AOUT output is high impedance during this period. No regular cell voltage measurement can be taken during this time period. However, the SPI operates normally when communicating with other devices (e.g., in daisy-chain mode). So as not to affect calibration, do not take measurement and keep the devices in sample mode ( $\text{ECS} = 0$ ,  $\text{SC2}$ )  $= 0$ ,  $\overline{\text{SMPLB}} = 0$ ). After power-up, if the devices do not calibrate regularly, a temperature offset drift of  $\pm 1.5$  $\mu$ V/°C can occur.

#### *Monitoring Less Than 12/16 Cells*

The devices can monitor from 3 ( $V_P > +6V$ ) to 12/16 cells ( $V_P < +65V$ ). When monitoring less than the maximum number of possible cells per device, connect the most negative cell stack voltage to the bottom of the voltage input string (CV0). The unused CV\_ inputs at the top of the string should be shorted together and connected to  $V_P$ . Leave the unused  $BA$ ,  $CT$ , and  $CB$ pins unconnected.

#### *Reading Total Cell Stack Voltage*

Besides monitoring the individual cell voltages, the devices can monitor the total voltage of the cell stack. An internal resistive voltage-divider between VP and AGND divides the stack voltage by 12 (MAX14920) or 16 (MAX14921). This provides a way to quickly determine the state of the total battery pack, as well as the average voltage of all cells. The settling time of AOUT is 60µs. To

### High-Accuracy 12-/16-Cell Measurement AFEs

read out the total cell stack voltage, set the [ECS, SC0, SC1, SC2, SC3] bits to [0, 0, 0, 1, 1]. The total cell stack voltage can be read during the sample or hold phase.

#### *SPI Serial Interface*

Control of the devices is done through a 24-bit SPI interface. The controller sends the serial data to the devices through the SDI input. The devices simultaneously send out monitoring data at the SDO output. This scheme allows daisy-chained operation with other daisy-chainable devices, such as ADC converters. [Figure 7](#page-16-0) shows the serial bit sequence.

CB1 is the first bit expected from the controller and C1 is the first bit that the devices sent to the controller. The SDO data changes on the falling edge of the SCLK signals. The devices sample the SDI data on the rising edge of SCLK.

#### *SPI Configuration/Control Bits*

The configuration/control bits allow enabling of the charge-balance switches, sampling and holding of all the cell voltages, selecting the cell for voltage output, selecting the T<sub>\_</sub> input channels, and enabling diagnostics mode. [Table 1](#page-16-1) describes the bits that the devices receive from the host controller for configuration and control through SDI.

<span id="page-16-0"></span>

*Figure 7. SPI Serial Interface Bits*

### <span id="page-16-1"></span>Table 1. SPI Configuration/Control Bits



# High-Accuracy 12-/16-Cell Measurement AFEs



### Table 1. SPI Configuration/Control Bits (continued)

\**Not available on the MAX14920. Setting the bit to 0 or 1 does not affect the operating of the MAX14920.* 

\*\**For the MAX14920, if n > 12,*  $V_{AOUT} = 0V$ *.* 

# High-Accuracy 12-/16-Cell Measurement AFEs

### Table 2. Cell Selection



\**For MAX14921 only.*

### Table 3. Analog Input Selection



# High-Accuracy 12-/16-Cell Measurement AFEs

#### *SPI Monitoring Bits*

The monitoring bits provide feedback of undervoltage conditions and thermal shutdown, as well as indication when the devices are ready for operation after power-up. [Table 4](#page-19-0) describes the diagnostics/monitoring bits that the devices send back to the host controller through the SDO output.

#### *Flexible Logic Interface*

The serial/parallel logic control interface logic levels can be defined to be in a range between +1.62V (min) and +5.5V (max). The voltage applied to the  $V_1$  pin defines the logic levels. Choose the  $V_1$  voltage to match the controller and ADC's I/O logic levels.

### <span id="page-19-0"></span>Table 4. SPI Monitoring Bits



\**Not available on the MAX14920. Setting the bit to 0 or 1 does not affect the operating of the MAX14920.* 

### High-Accuracy 12-/16-Cell Measurement AFEs

#### *Linear Regulator*

The internal linear regulator has LDOIN as its input voltage and regulates this down to  $+5V \pm 5%$  at the V<sub>A</sub> output with a load current of 10mA (max). The LDO is automatically enabled when LDOIN is above +5.5V. The internal LDO is short-circuit protected with a current limit higher than 14mA (22mA, typ). An external +5V regulator can be used instead of the internal one. When using an external +5V regular, LDOIN must be connected to VA.

#### *Thermal Protection*

The devices have thermal shutdown to protect them against thermal overheating. In thermal shutdown, the LDO, amplifier, and charge-balance circuitry stop operation. The SPI interface is functional in thermal shutdown.

#### *Shutdown Mode*

The devices can be placed into low standby-power shutdown mode through the LOPW bit. The internal LDO remains on and the amplifier disabled, bringing the VP supply current down to  $1\mu A$  (max).

#### *Analog/Temperature Inputs*

The T1, T2, and T3 inputs are single-ended, CV0 referenced, general-purpose analog inputs that are multiplexed to AOUT or to AOUT through a buffer [\(Figure 8](#page-20-0)). These inputs can be used for connection of temperature sensors or for a current monitor.

The total mux and switch series resistance is less than  $200Ω$ . In applications where the load current flowing to the AOUT output is so high that significant errors are introduced due to series resistance in the voltage source and/or the signal path, use the buffer amplifier to improve accuracy.

Route the T\_ inputs through the buffer to AOUT by setting the SPI bits [ECS, SC0, SC1, SC2, SC3] = [0, b, a, 1, 1]. Route the T\_ inputs directly to the AOUT output by setting the bits [ECS, SC0, SC1, SC2, SC3 = [0, b, a, 0, 1]. Bits a and b select one of the three T inputs or three-state the AOUT output.

#### *Three-Stating the AOUT Output*

The AOUT output can be three-stated to share this pin with other external signal sources, such as additional temperature sensors. Use the ECS and SC\_ bits to threestate the AOUT output.

#### *Charge Balancing*

Low-voltage enhancement-mode n-channel FETs can be connected for passive balancing of cells. Select low onresistance FETs with a  $V_T$  less than  $V_{BAH}$ . Connect the FETs between each cell's anode and cathode through a current-limiting resistor in the drain [\(Figure 9](#page-20-1)).

The charge-balancing FETs can be enabled through SPI control. An internal 600 $\Omega$  (typ)/900 $\Omega$  (max) pulldown resistor assures that the FET is normally switched off. When balancing is active, a leakage current of 5 $\mu$ A is sunk from CV\_. In addition, an internal balancing current flowing from CVn to CVn - 1 of 10mA (max) is present, where  $n = 1-12$  (MAX14920) and  $n = 1-16$  (MAX14921). The power dissipation created by the internal current during balancing should be considered for total package power management.

#### *Diagnostics*

The devices' integrated diagnostics allow detection of shorts between wires, as well as open-wire conditions of the CV\_ pins.

<span id="page-20-0"></span>

*Figure 8. Analog/ Temperature Measurement Figure 9. Charge Balancing*

<span id="page-20-1"></span>

### High-Accuracy 12-/16-Cell Measurement AFEs

Shorts between cell connections can be detected during normal operation. The cell readout voltage results in ~0V or ~VA depending on where the short happens. In the case of shorts, the maximum currents flowing in/out of the pins must be limited and overvoltages avoided, including the external components (balancing FETs and sampling capacitors).

Open-wire conditions between the CV\_ inputs and the cells can be detected in two different ways:

#### The first method of open-wire detection:

Set the DIAG bit to 1 while in the sampling phase. This applies a leakage current of 10µA to the CVn inputs. If CVn is unconnected, the leakage current starts discharging the sampling capacitor with a slew rate of  $I_{\text{I}}$   $FAK$ CSAMLPF  $(-10\mu A/1\mu F = 100\text{mV}/10\text{ms})$  down to CVn - 1. Two successive readouts show considerable cell voltage change in case of an open wire. Alternatively, waiting for a sampling time of ~300ms to 500ms reduces the cell voltage to below the UV\_VC $_{VTH}$  threshold voltage.

First open-wire detection procedure:

- Set DIAG bit to 1
- Wait  $> 0.5$ s before hold phase
- Read out the Cn bit or the CVn voltage under SPI control, where  $n = 1 - 12$  (MAX14920) and  $n = 1 - 16$ (MAX14921)

#### The second method of open-wire detection:

To check for a single open-wire connection, it is faster to enable the balancing FET only on the selected cell during the sampling phase and then reading out the selected cell voltage. If CVn is unconnected, the balancing FET rapidly (time depends on the balancing resistance used) shorts CVn to CVn - 1 and the readout phase shows ~0V or CVn and a voltage higher than  $V_A$  on CVn + 1.

Second open-wire detection procedure:

- Set the BAn bit to 1
- Wait for a time of RBAL x CSAMPLE before switching to the hold phase
- Route the CVn voltage to AOUT
- Repeat this procedure for all cells

During this procedure, the capacitors and external FETs need to withstand a voltage equal to  $V_{C}V_{n}$  -  $V_{C}V_{n-1}$ , where  $n = 1-12$  (MAX14920) and  $n = 1-16$  (MAX14921).

#### *Input-Voltage Clamping*

The devices have internal ESD-protection diodes that can clamp input voltage lower than AGND or higher than VP (CVn where  $n$  is  $> 1$ ) or 6 volts for (CV1) during a fault condition. Connect series resistors (RLIM) to the inputs to limit the currents flowing through the forward-biased diodes during fault conditions [\(Figure 10\)](#page-21-0). Choose current-limiting resistors so the input currents are limited to  $I_{CV}$  (max) = 10mA. The additional power dissipation due to the fault currents needs to be calculated when a voltage-clamping condition occurs on another channel that is not being measured. Sampling capacitors and balancing FETs must be chosen appropriately or protected with external voltage clamps to survive such events.

#### *Power Sequencing*

The  $V_A$  and  $V_I$  supplies can be applied at any sequence with respect to each other and also independently of the V<sub>P</sub> and supplies CV inputs. The V<sub>P</sub> voltage has to connect to the highest voltage of the cell stack.

<span id="page-21-0"></span>

*Figure 10. Input-Voltage Clamp*

# High-Accuracy 12-/16-Cell Measurement AFEs

### *Applications Information*

#### *Sampling Speed and Capacitor-Selection Considerations*

Capacitor values of  $1\mu$ F are recommended for achieving low errors and at high sampling rates, with sample and hold times in the order of 5ms. With 1µF capacitors and good PCB layout, charge injection-error correction is normally not required.

If higher/lower sampling speeds are required, the sampling capacitors and/or the series resistors at the cell connections can be reduced and/or increased.

The cell sampling capacitors connected to the CT\_ and CB\_ terminals affect:

- Speed of operation
- Cell readout accuracy

The smaller the sampling capacitor values, the lower their RC time constant and hence the faster their charging time. Therefore, for higher-speed operation, smaller capacitor values can be selected.

One application case can be when the cell voltages are known to only vary by small amounts from one sample to the next. In this case, the sampling capacitors can be made smaller, as the sampling phases only need to charge the capacitors by the charge lost during the previous level shift and hold phase, including the small change in cell voltage. See the *[Measurement Accuracy](#page-14-0)* section for details on how to calculate the voltage drop due to these two factors. For example, sampling capacitors of approximately 100nF can be adequate, thereby reducing the sampling phase by a factor of 10. If this technique is used, the initial sampling times, after initial power-up, either have to be made longer to allow the initially discharged sampling capacitors to charge up to the cell voltages, or the initial samples are disregarded until the monitored voltages stabilize to their final cell value.

The accuracy dependence on the capacitor values is determined by the discharge during the hold phase and by the errors introduced during level shifting (both were previously described). By speeding up the readout of the cell voltages during the hold phase, discharging is reduced. Note that the last cell voltage being read out is most affected by discharging, due to its longer hold delay until being read out. Smaller capacitor values are prone to higher charge injection errors caused by level shifting. Both low-capacitance layout and level-shift compensation reduce these errors.

#### *Typical Application Circuit*

[Figure 11](#page-23-0) shows a high-accuracy measurement application based on an accurate 16-bit ADC, together with a high-quality voltage reference. The internal linear regulator is used for supplying  $V_A$  (+5V), and uses the SAMPL input for controlling the cell voltage sample and hold times. Thermistors are connected to the T1, T2, and T3 inputs to monitor three temperatures.

If less absolute measurement accuracy is acceptable, an ADC with internal reference, such as the MAX11163, can be used. In applications where accuracy is not a critical factor, a microcontroller's internal ADC may be adequate.

#### *Multipack Applications*

In applications that require more than 12/16 cells to achieve higher voltages, multiple cell packs can be stacked. Each pack in the stack does not have to have the same number of cells. A minimum of +6V or 3 cells can be monitored by the devices.

In stacked packs, the sample signal can either be centrally controlled by a common signal for simultaneous sampling, or the sample/hold can be initiated through SPI. Two cell packs stacked on one another can be interconnected through an SPI or other communication interface. The packs can either have internal controllers or multiple packs can be controlled by one common controller. Internal controllers perform autonomous calibration and measurements, and allow an external controller to collect the data on demand. This scheme is shown in [Figure 12](#page-24-0). To translate the interpack communication signals between the differing common-mode pack voltages, use opto-isolators, digital isolators, or digital ground level shifters [\(Figure 12\)](#page-24-0).

#### *Layout Considerations*

Keep the PCB traces to the sampling capacitors as short as possible and minimize parasitic capacitance between the capacitor pins and the ground plane.

# High-Accuracy 12-/16-Cell Measurement AFEs

<span id="page-23-0"></span>

*Figure 11. Typical Application Circuit*



<span id="page-24-0"></span>

*Figure 12. Stacked Battery Pack Application Diagram Based on Daisy-Chained SPI*

# High-Accuracy 12-/16-Cell Measurement AFEs

### *Functional Diagram*



# High-Accuracy 12-/16-Cell Measurement AFEs



+*Denotes a lead(Pb)-free/RoHS-compliant package.* \**EP = Exposed pad.*

### *Chip Information*

PROCESS: BiCMOS

### *Ordering Information Package Information*

For the latest package outline information and land patterns (footprints), go to **<www.maximintegrated.com/packages>**. Note that a "+", "#", or "-" in the package code indicates RoHS status only. Package drawings may show a different suffix character, but the drawing pertains to the package regardless of RoHS status.



### High-Accuracy 12-/16-Cell Measurement AFEs

### *Revision History*





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